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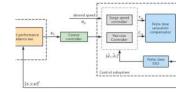
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Journal of Marine Science and Technology > Aims and scope

Aims and scope

The sea is where life is said to have originated. Not only do the earth's oceans provide vital routes of transportation and a rich source of raw materials; they have also remained a challenging frontier and an essential natural habitat whose preservation will be crucial to human survival in the twenty-first century. The efforts of marine scientists and technologists are aimed at the advancement of scientific and engineering knowledge regarding the sea.

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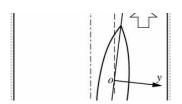
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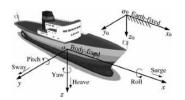
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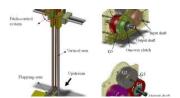


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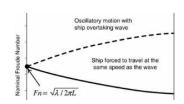


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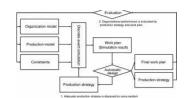
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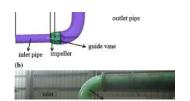
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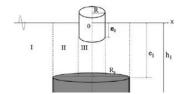
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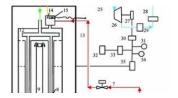


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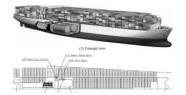
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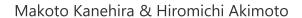
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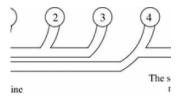
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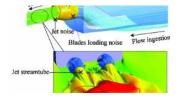


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ORIGINAL ARTICLE

Optimization of P.E. area division and arrangement based on product mix

Sanghwan Kim · Hyun Chung · Mingyu Kim

Received: 25 December 2012/Accepted: 1 May 2014/Published online: 29 May 2014 © JASNAOE 2014

Abstract The shipbuilding industry in recent times has witnessed a decline in the demand for commercial ships and a sharp increase in the demand for offshore plants. In response to this change in the industry, shipbuilding companies have sought an optimal product mix for producing commercial ships and offshore plants with minimal additional investment in facilities. This study was aimed at optimizing the pre-erection (P.E.) area partition for ship and offshore blocks based on the forecasted product mix of the planning horizon. The offshore P.E. area requires additional investment in facilities because the blocks are usually much heavier than those of ships. For given production schedules, and taking the flexibility of the forecasted change into consideration, we determined the optimal P.E. area partition ratio using the dynamic layout problem methodology. In this study, material handling cost, operating cost, rearrangement cost, and additional P.E. area construction cost were used to determine the optimal division. The optimal division of the P.E. area for offshore plants was then determined for a 10-year planning horizon. The results were applied to a shipyard to evaluate their business feasibility.

Keywords Product mix · Layout · Pre-erection area · DLP (dynamic layout problem) · Optimization · Shipyard

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1 Introduction

The demand for deep-sea drilling ships has increased in recent times owing to the greater demand for oil and higher oil prices. To fulfill the demand for offshore plants, many studies are being conducted by shipyards to enable the mixed production of ships and offshore plants in the workspace for commercial ships, the demand for which has dropped. Product mix is a production strategy that adds a different product to the production line while minimizing investment in additional facilities. To achieve product mix for commercial ships and offshore plants, various factors such as the block schedule, weight, size, and erection method must first be examined. Figure 1 shows a product mix process for a shipyard. Product mix processes for commercial ships and offshore plants include cutting, fabrication, flat assembly, and curve assembly. However, given the characteristics of commercial ships and offshore plants, the building process is more commonly separated from the pre-erection (P.E.) process. A block is the basic unit in shipbuilding. One method for reducing the assembly time within the building dock involves the formation of a grand block by pre-assembling several blocks and then transferring it to the dock for erection. Whereas the number of grand blocks may differ depending on the shipyard, approximately 10 are used to build a ship [1].

The sizes and weights of the ship blocks and offshore plants are determined by the product development conditions of the company, factory size, and strategic decisions. Since offshore plants are equipped with drilling derricks, external turret mooring systems, and other heavy equipment, an offshore plant block tends to be heavier than the block of a commercial ship. The former is also larger than the latter thus the erection of an offshore plant is done outside a dock and there are less size constraints.



ORIGINAL ARTICLE

Parametric bulbous bow design using the cubic Bezier curve and curve-plane intersection method for the minimization of ship resistance in CFD

Deddy Chrismianto · Dong-Joon Kim

Received: 3 April 2013/Accepted: 6 June 2014/Published online: 5 July 2014 © JASNAOE 2014

Abstract Parametric geometric modeling plays an important role in ship's hull form optimization by use of computational fluid dynamic (CFD) analysis. However, it is difficult to create satisfactory parametric modeling for some curved shapes, such as a ship's bulbous bow. In this study, the cubic Bezier curve and curve-plane intersection methods are applied to generate the parametric design of a bulbous bow in a solid modeling procedure by taking into account the input of 4 (four) design parameters. For this, a suitable application program interface script within the ANSYS Design Modeler was developed. An application to the ship resistance minimization by use of CFD was made to show that the proposed method could be implemented properly. In this respect, the parametric design of the bulbous bow of a container ship (KRISO Container Ship type) was chosen to be modified. First, it was shown that the computational results generated by CFD were close to the experimental data for the original ship hull form. The developed optimization method was subsequently applied to find the optimal bulbous bow. Finally, the dependence of the optimum bulbous bow on a ship's speed (some variations of Fn values) was investigated and the results were compared to each other.

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Department of Naval Architecture and Systems Marine Engineering, Pukyong National University, Busan, South Korea e-mail: djkim@pknu.ac.kr **Keywords** Parametric bulbous bow design · Cubic Bezier curve · Curve-plane intersection method · CFD · Optimization method

1 Introduction

Recently, the relationship between parametric design and ship performance analysis using computational fluid dynamic (CFD) has become a topic of interest, specifically, how to obtain an optimum ship hull form or an optimum bulbous bow form that will ensure a ship's good hydrodynamic performance. There are several methods of parametric design that have been used in ship modeling. The use of the control points of the cubic B spline to generate the parametric of ship hull design as well as the parametric of bulbous bow design has been introduced with successful results [1-5]. Campana et al. [6] has used the Bezier polynomial patches method, in which the shape modification was controlled by a given number of control points that were used as design variables/input parameters for finding an optimum shape in the optimization process. Chen and Huang [7] has used a technique for parameter estimation using the B-spline surface fitting method in the inverse design problem of finding the optimal hull form. In addition, Kang and Lee [8] has implemented the parametric morphing technique to generate hull form rapidly with some variations of the input parameters. Furthermore, Rodriguez and Jambrina [9] has developed a programmed design based on a programming language as a tool for parametric hull form generation. In general, these methods can be used to create the parametric design for surface modeling only. However, some CFD softwares (especially RANSE solver) need a solid modeling in the meshing stage before the CFD analyzing stage can begin. Pecot et al. [10]



ORIGINAL ARTICLE

Numerical prediction of the fluctuating noise source of waterjet in full scale

Qiongfang Yang · Yongsheng Wang · Zhihong Zhang

Received: 21 May 2013/Accepted: 8 March 2014/Published online: 29 March 2014 © JASNAOE 2014

Abstract Fluctuating noise sources of the full-scaled waterjet equipped on the transom of a trimaran at 18 kn are analyzed by hybrid method coupling Scale-Adaptive Simulation (SAS) of periodic pulsating pressure on blades with boundary element acoustic models (BEM) for acoustic field. Numerical self-propelled tests of the full-scaled trimaran-waterjet system using $k - \varepsilon$ explicit algebraic Reynolds stress turbulent model (EARSM) with rotationcurvature correction are completed to output the non-uniform inflow into waterjet. The total propulsive efficiency is predicted satisfactorily, and local flow details are reasonably reproduced. Transient simulations of the fluctuating pressure of waterjet pump with non-uniform inflow at selfpropelled rotating speed reveal that: pulsating pressure of the monitoring points located at the back of the rotor and before the stator presents the most dominant second blades passing frequency (BPF) line spectrum in frequency domain to reflect the rotor-stator interaction. When 0.95 times of span is used to represent the most heaviest loading section on rotor blades, the averaged pulsating pressure coefficient at BPF per unit chord is far more smaller than that on propeller blades. The acoustic highlights of the sound intensity distribution in the pump are located in the axial region between rotor with stator at BPF and its harmonics. The most-dominated tonal noise at 2BPF is 136.2 dB, and the total sound pressure level over the range of 1 kHz is 148.8 dB with scattering effect of the hull stern

involved. Comparing to the propeller with a comparative absorbed power, smaller non-uniformity of inflow and smaller pulsating pressure benefits the waterjet about 16 dB quieter noise.

Keywords Numerical self-propulsion · Waterjet noise · Fluctuating pressure · Full scale

Abbreviations

List of symbols

D Diameter of pump inlet (mm)

G Sound Green's function

K Turbulent kinetic energy (m^2/s^2)

 $K_{\rm p}$ Non-dimensional fluctuated pressure coefficient

 $n_{\rm s}$ Specific speed of pump

n Propeller rotating speed (r/s)

 $p(\mathbf{r})$ Sound pressure at any position \mathbf{r}

P Braked power (kW)

Q Volume flow rate (m^3/s)

T Thrust deduction coefficient

T Thrust of the waterjet (N)

v_s Uniform incoming velocity, ship speed (m/s)

v⁺ Dimensionless normal distance from the wall

Greek symbols

 α_v Air volume fraction

 $\mu_{\rm t}$ Turbulent viscosity

 ω Turbulent vortex frequency

 Ω Vorticity tensor, second invariant of velocity gradient

 σ Sinkage coefficient

τ Retarded time, flow time-scale

 δ Trim coefficient

ζ Flow non-uniform level

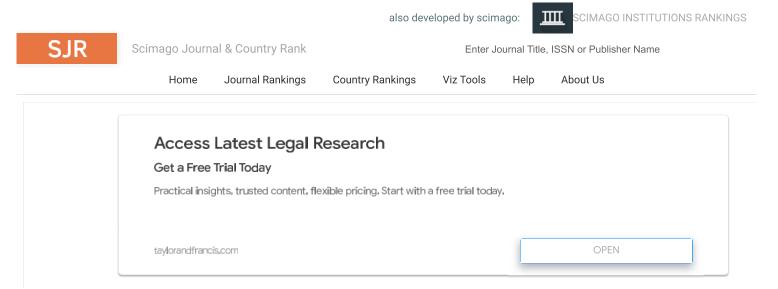
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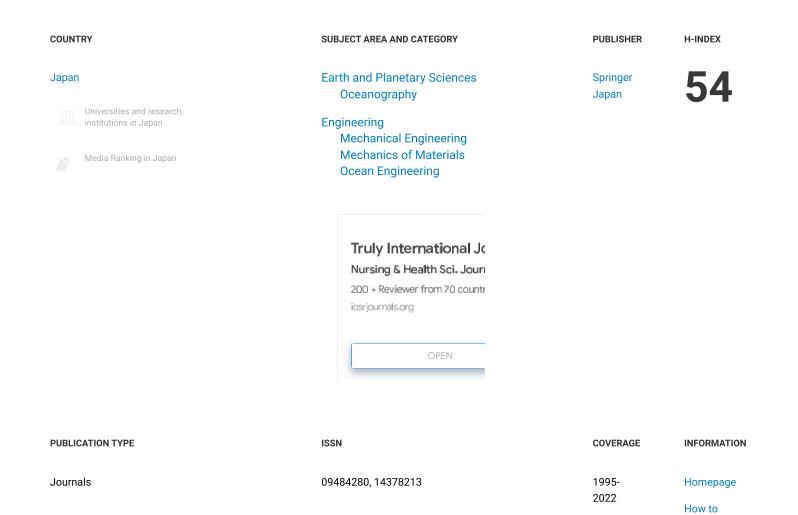
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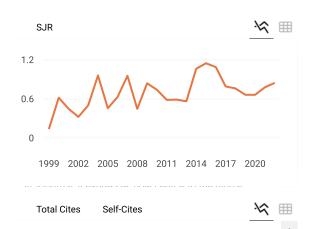
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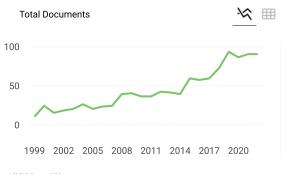
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