BUKTI KORESPONDENSI

| No. | Kegiatan | Tanggal |
|-----|--|------------|
| 1. | Pengiriman draft publikasi pertama (Bukti penerimaan draft | 14-4-2020 |
| | publikasi dari team editor) | |
| 2. | Permintaan revisi untuk draft yang dikirim ke jurnal | 11-5-2020 |
| 3. | Perbaikan draft publikasi dari penulis | 17-5-2020 |
| 4. | Permintaan revisi dari editor terhadap hasil perbaikan pertama | 29-6-2020 |
| 5. | Perbaikan draft publikasi atas koreksi dari editor | 7-7-2020 |
| 6. | Draft publikasi dinyatakan diterima untuk dipublikasikan | 15-7-2020 |
| 7. | Permintaan copyediting dari editor | 26-10-2020 |
| 8. | Pengiriman draft hasil copyediting dari penulis | 30-10-2020 |
| 9. | Penerimaan draft hasil copyediting oleh editor | 30-10-2020 |
| 10. | Permintaan proofreading draft sebelum naskah terbit | 24-11-2020 |
| 11. | Penulis menyetujui versi proofreading | 24-11-2020 |
| 12. | Draft memasuki proses produksi untuk penerbitan | 25-11-2020 |
| 13. | Naskah publikasi terbit | 1-12-2020 |

1. Pengiriman draft publikasi pertama (Bukti penerimaan draft publikasi dari team editor)

Prof. Dr. Ir. Komang G. Wiryawan <jurnal@apps.ipb.ac.id> To: sutaryo



sutaryo sutaryo:

P

Thank you for submitting the manuscript, "A Performance Comparison of Single and Two Phase Biogas Digesters Treating Dairy Cattle Manure at Tropical Ambient Temperature" to Tropical Animal Science Journal. With the online journal management system that we are using, you will be able to track its progress through the editorial process by logging in to the journal web site:

Manuscript URL: <u>https://journal.ipb.ac.id/index.php/tasj/authorDashboard/submission/30343</u> Username: soeta

If you have any questions, please contact me. Thank you for considering this journal as a venue for your work.

Prof. Dr. Ir. Komang G. Wiryawan

__ Tropical Animal Science Journal

http://journal.ipb.ac.id/index.php/tasj

Cover letter 1 dan draft versi pertama kali dikirim

The Editor(s),

14th April, 2020

Tropical Animal Science Journal,

Dear Sir/Madam,

Subject: Submission of manuscript titled 'Performance Comparison of Single and Two Phase Biogas Digesters treating Dairy Cattle Manure at Tropical Ambient Temperature'

- authored by Sutaryo Sutaryo, Aldila Nugrahaini Sempana, Cristina Maria Sri Lestari, Alastair James Ward

We herewith submit our paper with the title **Performance Comparison of Single and Two Phase Biogas Digesters treating Dairy Cattle Manure at Tropical Ambient Temperature**. The manuscript is an original research based on experiments carried out during 2018 at Diponegoro University, Indonesia and has not been previously submitted to any other journal.

The objective of this experiment has been to evaluate the effect of different biogas digester configurations (single and two-phase) on methane production of dairy cattle manure (DCM) at tropical ambient temperature. It has been demonstrated that there was no positive effect with the application of a two-phase digester configuration on specific methane yield of DCM per kg volatile solids added. Methane production was detected in the first reactor of the two-phase digester configuration and the total sum methane production of the two-phase digester was found to be 29.98% higher than that of the single reactor in terms of digester volume. Both digester configurations performed well, indicated by stable methane production, low volatile fatty acids and total ammonia concentrations.

We agree on the contents of the manuscript and would like to submit our manuscript to **'Tropical Animal Science Journal'**

Thank you and best regards,

On behalf of all the authors,

Sutaryo Sutaryo Faculty of Animal and Agricultural Sciences Diponegoro University Tembalang-Semarang 50275, Indonesia Email: <u>soeta@lecturer.undip.ac.id</u>; <u>sutaryoundip@yahoo.com</u>

| 1 | Performance Comparison of Single and Two Phase Biogas Digesters Treating |
|----|---|
| 2 | Dairy Cattle Manure at Tropical Ambient Temperature |
| 3 | |
| 4 | S. Sutaryo ^a *, A. N. Sempana ^a , C. M. S. Lestari ^a , A. J. Ward ^b |
| 5 | |
| 6 | ^a Department of Animal Science, Faculty of Animal and Agricultural Sciences, |
| | |
| 7 | Diponegoro University, Semarang, Indonesia |
| o | ^b Department of Engineering Faculty of Science and Technology Aarbus University |
| 0 | Department of Engineering, Faculty of Science and Technology, Aamus Oniversity, |
| 9 | Aarhus, Denmark |
| | |
| 10 | *Corresponding author: soeta@lecturer.undip.ac.id; sutaryoundip@yahoo.com |
| | |
| | |

ABSTRACT

| 12 | This study examined the effect of different biogas digester configurations (single |
|----|---|
| 13 | and two-phase) on methane production of dairy cattle manure (DCM) at tropical ambient |
| 14 | temperature. The results showed that there was no positive effect with the application of |
| 15 | a two-phase digester configuration on specific methane yield of DCM per kg volatile |
| 16 | solids added. Methane production was detected in the first reactor of the two-phase |
| 17 | digester configuration and the total sum methane production of the two-phase digester |
| 18 | was found to be 29.98% higher (p<0.05) than that of the single reactor in terms of digester |
| 19 | volume. Both digester configurations performed well, indicated by stable methane |
| 20 | production, low volatile fatty acids and total ammonia concentrations. |
| 21 | Key words: biogas, manure, tropical ambient temperature, two-phase digester biogas. |
| | |

INTRODUCTION

The dairy cattle industry produces large amounts of waste in the form of manure that can cause environmental pollution if not managed properly. Daily dairy cattle manure (DCM) (wet feces plus urine) excretion is 89.0; 65.9; 34.8 kg/d per 1000 kg of body weight for those that produce 29 and 14 kg/d of milk and for non-lactating dairy cows, respectively (Wilkerson *et al.*, 1997). Generally, animal waste management can take place in aerobic condition through a composting process or by anaerobic digestion (AD) to produce biogas.

Manure management through the AD process results in numerous advantages 33 including the generation of renewable energy in the form of biogas. Biogas is the most 34 35 efficient and effective among the various alternative sources of energy currently available, it needs less capital investment per unit production cost compared to other 36 37 renewable energy sources and it is available as a domestic resource in the rural areas, therefore it is not subject to world price fluctuations (Rao et al., 2010). In addition, biogas 38 production from animal manure can creates new enterprises and increases the income in 39 40 rural area since it requires labour for production, collection and transport of AD 41 substrates, manufacture of technical equipment and the construction, operation and maintenance of biogas plants (Adekunle and Okolie, 2015). 42

Technically, the AD process can take places in three different temperature ranges: (1) psychrophilic (cryophilic) temperature from 10 to 20°C; (2) mesophilic temperature from 20 to 40°C; and (3) thermophilic temperature from 40 to 60°C (Burton and Turner, 2003). Based on those temperature range criteria, the AD process can be implemented at tropical ambient temperatures. Moreover, operation of AD at tropical ambient temperatures offers advantages compared to the operation of AD under mesophilic or

thermophilic temperatures, since AD operation at higher temperatures require significant energy to maintain bioreactor temperature (Bandara *et al.*, 2012).

50

Among other biogas digester designs, the continuously stirred tank reactor 51 (CSTR) design is the most commonly applied bioreactor for treating agricultural waste 52 53 (Linke et al., 2015). While in operation, the process of biodegradation of organic waste can be in single or two-phases. The two-phase AD process has several advantages 54 compared to single phase. These include the selection and enrichment of different bacteria 55 in each digester, increasing the stability of the process by controlling the acidification 56 stage therefore reducing the risk of overloading and the buildup of toxic material. The 57 first stage in the two-phase configuration can act as metabolic buffer preventing pH shock 58 to the methanogenic microorganisms and low pH in the first stage due to a high organic 59 loading rate favours the establishment of the acidogenic phase (Sinbuathong et al., 2012). 60 Although previous studies have evaluated the AD process at ambient temperature (Minale 61 and Worku, 2014; Wei et al., 2014; Murrugan and Appavu, 2018) and two phase AD 62 (Baldi et al., 2019; Tsigkou et al., 2020), to the best of our knowledge there has been a 63 64 lack of information regarding direct comparison of single and two phase AD of DCM at 65 tropical ambient temperature. Therefore the aim of this current study was to further knowledge in this specific area. 66

67

- 68
- 69

MATERIALS AND METHODS

Experimental Set Up

Evaluation of single and two phase processes was conducted using three identical digesters (R1, R2, R3). The reactors were made from stainless steel and in order to minimize temperature fluctuations between day and night time, all digesters were made with double layers. The two phase digesters consisted of reactors R1 and R2. Reactor 1
had a 2.1 L working volume (the minimum volume that can be applied in the reactor) and
3 d hydraulic retention (HRT) while R2 had 5.25 L working volume and 22 d HRT.
Therefore in total R1 and R2 had a 25 d HRT. R3 served as the single phase bioreactor
and had 5.25 L working volume and 25 d HRT. Mao *et al.* (2015) reported that under
mesophilic conditions an average HRT in the range of 15-30 d is required to treat waste.

The experiment was started by filling R1 with 1.4 kg inoculum and 0.7 kg DCM, 79 R2 with 5.011 kg inoculum and 0.239 kg DCM and R3 with 5.040 kg inoculum and 0.210 80 kg DCM. From the second day, all digesters were fed as follows: 0.7, 0.239 and 0.210 kg 81 DCM for R1, R2 and R3 respectively (after first removing the same amount of digestate 82 from a port at the base of the digesters) which continued for the following 21 d adaptation 83 period. The digesters were fed through a tube, the outlet of which was submerged under 84 the substrate level to avoid air ingress during the feeding process. Data were collected 85 after this 21 d startup period. During the data collection period, R1 was fed 0.7 kg DCM. 86 Effluent from this digester (0.239 kg) was used to feed R2, while R3 was fed 0.210 kg 87 DCM. Digesters were kept at ambient temperature and the experiment was run for a 88 89 period of three HRT corresponding to 75 d in total.

90

91

Inoculum and Substrate

92 Inoculum in this study was sourced from the active biogas digester at the Faculty 93 of Animal and Agricultural Sciences, Diponegoro University. The digester treats DCM 94 and operates at ambient temperature. The digestate slurry from the digester was 95 transferred directly to the laboratory scale digesters. Substrate was taken from dairy cows in the lactation period and was collected
from the farm in Faculty of Animal and Agricultural Sciences, Diponegoro University.
Manure was diluted with tap water in the ratio 1:1.5. Manure was collected once per week
and diluted with tap water directly and kept refrigerated. pH value, volatile solids (VS)
and total ammonia nitrogen (TAN) concentration in the inoculum were 7.11, 7.33% and
265.18 mg/L respectively, while pH value, VS, TAN and volatile fatty acids (VFA) (C2C5) concentration of DCM were 6.77, 7.40%, 97.98 mg/L and 142.93 mg/L respectively.

- 103
- 104

Analytical Methods

Biogas from the laboratory scale bio-digesters was passed up through 0.5 L 105 106 infusion bottles that contained 4% NaOH solution in order to absorb CO₂ using 5 ml diameter Teflon tubing. Methane production was measured on a daily basis by collecting 107 the gas using 5 L tedlar gas bags using a water displacement method (Figure 1). The 108 procedures to quantify gas production were: 1) valve to pump was in open position. 2) 109 110 water pump was switched on, therefore air in the measuring glass head space was 111 removed and the head space was filled up with tap water. 3) valve to pump was closed. 4) water pump was switched off. 5) valve to tedlar gas bag was opened therefore the 112 methane in the tedlar gas bag will move to the head space of the measuring glass. 6) gas 113 114 volume was read in the measuring glass scale. When the gas volume in the tedlar gas bag exceeded the measuring glass volume, steps 1-6 were repeated. The net gas production 115 was corrected to STP conditions. 116

Daily maximum and minimum ambient temperature was recorded using a digital
hygrometer thermometer HTC-2 (Taiwan). Sample pH value was measured using a pH
meter (Hanna® pH meter). Dry matter (DM) contents of samples were analyzed by drying

| 120 | at 105°C for 7 h. Ash was determined by combusting the dried samples at 550°C for 6 h |
|-----|--|
| 121 | and VS was calculated by subtracting the ash weight from the DM (APHA,1995). TAN |
| 122 | concentration was measured using photometric kits (HACH® USA: DOC316.53.01077) |
| 123 | at 655 nm. VFA were determined using gas chromatography (Shimadzu GC-8). The |
| 124 | collected data were statistically analyzed using ANOVA with 95% confidence level. |
| 125 | Duncan's multiple range tests were used in post ANOVA analysis when differences were |
| 126 | found to be significant (Gomez and Gomez, 2007). |
| 127 | |
| 128 | RESULTS |
| 129 | Ambient Temperature Variation |
| 130 | Average daily maximum-minimum ambient temperature throughout the |
| 131 | experiment was 36.55°C and 20.93°C respectively (Figure 2). There was 15.63°C |
| 132 | temperature difference between maximum temperature in day time and minimum |
| 133 | temperature in the night time and the ambient temperature in this study therefore falls into |
| 134 | the mesophilic category (Burton and Turner, 2033). |
| 135 | |
| 136 | Methane production |
| 137 | The methane production of the three bio-digesters throughout the experiment is |
| 138 | presented in Figure 3. The mean methane yields were 14.31 L kg/VS, 132.82 L kg/VS, |
| 139 | and 146 L kg/VS for R1, R2 and R3 respectively Total methane yield of R1 and R2 (R_{TS}) |
| 140 | was 147.13 L kg/VS (Table 2). A study from Amon et al. (2007) using batch digesters |
| 141 | with 60 d incubation period at 38°C showed that methane production of DCM from cows |
| 142 | with medium milk production was 166.3 N L kg/VS while the study from Sutaryo et al. |
| 143 | (2014) using continuous digesters with 20 d HRT at 35°C found that methane production |

| 144 | of DCM was 177 L kg/VS. Both those studies were performed at constant mesophilic |
|-----|---|
| 145 | temperature while the study presented here was performed at ambient variable mesophilic |
| 146 | temperatures, however the result of this study is similar with those previous results. |
| 147 | |
| 148 | Parameters in the Liquid Phase |
| 149 | Total VFA concentration and pH value of digested slurry are presented in Table |
| 150 | 1. The mean total VFA concentration was 160.74; 48.23; 39.19 mg/L for R1, R2 and R3 |
| 151 | respectively. Total VFA concentration of digested slurry in R1 was significantly higher |
| 152 | (p<0.05) than that in R2 and R3 (Table 1). TAN concentration concentrations of digested |
| 153 | slurry in this study were 137.85; 178.96; 185.86 mg/L for R1, R2 and R3 respectively |
| 154 | (Table 2). |
| 155 | Volatile solid reductions in this study were 29.85 and 28.03% for R2 and R3 |
| 156 | respectively. Study from Bhattacharya et al. (1996) found a VS reduction of 26% and |
| 157 | 30% for conventional and two-phase digester respectively treating sludges from |
| 158 | conventional activated sludge treatment plants and maintained at 35°C. Meanwhile a |
| 159 | study from Sutaryo et al. (2012) found a VS reduction in range of 27-35% for a reactor |
| 160 | treating DCM with different TS concentrations. Therefore the result of this study is in |
| 161 | accordance with the result of the previous study. |
| 162 | |
| 163 | DISCUSSION |
| 164 | Ambient Temperature Variation |
| 165 | This study was performed in July-September and in Indonesia that period is |
| 166 | considered to be in the dry season. A large variation temperature in AD operation in the |
| 167 | course of this study therefore has an adverse impact on the microorganism activity. Sakar |
| | |

et al. (2009) reported that the AD process is carried out by a prime balanced population
of various microorganisms. These microorganisms are very sensitive to environmental
condition changes including temperature.

- 171
- 172

Methane production

There was no significant effect (p>0.05) of the application of a two phase bio-173 digester on specific methane yield in terms of kg VS of substrate added when compared 174 to that from the single digester configuration (Table 1). However, methane production of 175 RTS was significantly higher (p<0.05) than that in R3 in term of L/L digester volume 176 (methane production/volume active). No significant effect (p>0.05) of the application of 177 178 the two-stage digester than single digester on specific methane yield in this study can be due to anaerobic microorganisms activities in both reactors configuration operation 179 efficiently. This study used digested slurry from an active digester that operated at a 180 tropical ambient temperature, the same condition used in this study. This fact, along with 181 the three weeks adaptation period contributed to the efficient microorganism's activity in 182 183 both reactor configurations in this study even though there was large temperature difference between day and night time. A study by Chae et al. (2008) found that using 184 batch digesters and treating swine manure, the methane production at 30 and 35°C were 185 186 quite similar, but it was higher by more than 13-17% than that at 25°C. Temperature 187 shocks caused a reduction in the methane production rate compared to that of the control, but it recovered rapidly. Once adapted, no significant effect on the methane production 188 189 was observed between the control and the temperature shock bio-digester. This fact therefore indicates that, even though methanogenic archaea are quite sensitive to 190

temperature shock they have considerable ability to adapt to temperature changes (Chae*et al.*, 2008).

Methane production in term of digester volume of RTS was 29.98% higher than 193 that in R3. The positive effect (p < 0.05) of the application of two phase digestion on the 194 195 methane production compared to that in the single phase reactor can be attributed to a shorter HRT period in R1 and R2 than that in R3, therefore the amount of substrate added 196 to R1 and R2 was higher than that in R3. Since the amount of substrate added to R2 (0.239 197 kg) was higher than that in R3 (0.210 kg) and in the same time the active volume in both 198 digester configurations was equal (5.25 L) therefore methane production in term of 199 digester volume R2 was higher than that in R3. In fact methane production in RTS was 200 201 methane yield in R1 and in R2. In this present study, HRT in R1, R2 and R3 were 3 d, 22 d and 25 d respectively. Bhattacharya et al. (1996) reported that one of the advantages of 202 phase separation is the ability to handle a higher organic loading rate than that in a single 203 reactor. A similar study from Tsigkou et al. (2020) found the same phenomenon, in that 204 205 the application of a two-stage digester treating co-digestion of used disposable nappies 206 and expired food product at 60:40 (v/v) ratio, working at mesophilic condition $(37\pm0.5^{\circ}C)$ 207 and 15 d HRT the energy production was 18.5% higher than that in the single reactor.

208

209

Parameters in the Liquid Phase

During bioconversion of organic matter in AD system there are four steps, namely hydrolysis, acidogenesis, acetogenesis and methanogenesis. In a two stage digester configuration, the first digester serves as the acidogenic phase (Sinbuatong *et al.*, 2012), therefore the VFA concentration will be higher than that in the second digester. A higher total VFA concentration in R1 than that on other reactor in this study is in accordance with Baldi *et al.* (2019) who found that total VFA concentration of digested slurry in a
fermentative digester was significantly higher than that of digested slurry from
methanogenic digester.

The higher VFA concentration of R1-digested slurry gave consequences on the lower pH value (p<0.05) than that in R2 and R3-digested slurry. The mean pH values of digested slurry in this recent study were 6.46; 6.84 and 6.89 for R1, R2 and R3 respectively. The pH value of R2 and R3 in this recent study was in the range of a stable AD process. Mao *et al.* (2015) reported that the ideal pH value for AD process is in the range of 6.8 to 7.4.

Ammonia is one of the essential nutrients for the growth of microorganisms, 224 225 however it can inhibit the AD process if it is available at high concentrations (Yenigün and Demirel, 2013). Under mesophilic conditions (35°C), the TAN inhibitory threshold 226 was in the concentrations of around 1700-1800 mg L-1 for unacclimated inoculum 227 (Yenigün and Demirel, 2013). TAN concentration of digested slurry in R1 was 228 229 significantly lower (p<0.05) than that in R2 and R3. This fact can be attributed to a shorter 230 HRT in R1 than that in R2 and R3 therefore microorganisms in R2 and R3 can degrade 231 more protein in the substrate, subsequently producing more ammonia. However TAN concentrations of digested slurry from all digester in this study were below the inhibitory 232 233 level as reported by Yenigün and Demirel (2013).

There was no significant effect (p>0.05) of the application two stage compared to single stage digesters on the VS reduction. No significant effect of phase separation on volatile solid reduction in this study suggests that microorganisms in both reactor configurations can work well.

CONCLUSION 239 It has been demonstrated that the application of a two-phase digester treating 240 241 DCM working at tropical ambient temperature significantly increased methane production by 29.98% compare to the single stage reactor in term of digester volume. 242 However, no significant effect of this digester configuration on specific methane yield in 243 terms of VS. Both digester configurations can run properly with stable methane 244 production, low VFA and TAN concentrations. Therefore the two-phase digester 245 246 configuration in tropical ambient temperature can be applied to increase methane production in term of digester volume. 247 248 249 **CONFLICT OF INTEREST** We certify that there is no conflict of interest with any financial, personal, or other 250 relationships with other people or organization related to the material discussed in the 251 252 manuscript. 253 254 ACKNOWLEDGEMENT The authors would like to thank Diponegoro University (grant number: 255 256 109/UN7.5.5/PP/2018) for financing this study. 257 258 REFERENCES Adekunle, K. F. & J. A. Okolie. 2015. A Review of Biochemical Process of Anaerobic 259 260 Digestion. Adv. Biosci. Biotechnol. 6:205-212.

| 261 | Amon, T., B. Amon, V. Kryvoruchko, W. Zollitsch, K. Mayer, & L. Gruber. 2007. |
|-----|---|
| 262 | Biogas production from maize and dairy cattle manure-Influence of biomass |
| 263 | composition on the methane yield. Agric Ecosyst Environ. 118:173-182. |

.....

- APHA, 1995. Standard Methods for Examination of Water and Waste Water, 19th ed.
 American Public Health Association, Washington, DC.
- Bhattacharya, S. K., R. L. Madura, D. A. Walling, & J. B. Farrell. 1996. Volatile
 solids reduction in two-phase and conventional anaerobic sludge digestion. Water
 Res. 30(5):1041-1048.
- 269 Bandara, W. M. K. R. T. W., T. Kindaichi, H. Satoh, M. Sasakawa, Y. Nakahara,
- M. Takahashi, & S. Okabe. 2012. Anaerobic treatmentofmunicipal wastewater
 at ambient temperature: Analysis of archaeal community structure and recovery
 of dissolved methane. Water Res. 46:5756-5764.
- Baldi, F., L. Pecorini, & R. Iannelli. 2019. Comparison of single-stage and two-stage
 anaerobic co-digestion of food waste and activated sludge for hydrogen and
 methane production. Renew Energy. 43:1755-1765.
- 276 Burton, C.H. & Turner, C., 2003. Anaerobic treatment options for animal manures. In:
- Manure Management Treatment Strategies for Sustainable Agriculture, 2nd edn,
 chapter 7. Silsoe Research Institute, as part of the EU Accompanying Measure

279 project, MATRESA, Wrest Park, Silsoe, Bedford, UK.

- Chae, K. J., S. K. Am Jang, L. Yim, & S. Kim. 2008. The effects of digestion
 temperature and temperatureshock on the biogas yields from the mesophilic
 anaerobic digestion of swine manure. Bioresour. Technol. 99:1-6.
- Gomez, K. A., & A. A. Gomez. 2007. Prosedur statistik untuk penelitian pertanian.
 Translated by Sjamsuddin, E., & J. S. Baharsjah. UI Press, Jakarta.

- Linke, B., A. Rodríguez-Abalde, C. Jost, & A. Krieg. 2015. Performance of a novel
 two-phase continuously fed leach bed reactor for demand-based biogas
 production from maize silage. Bioresour. Technol. 177:34-40.
- Mao, C., Y. Feng, X. Wang, & G. Ren. 2015. Review on research achievements of
 biogas from anaerobic digestion. Renew. Sust. Energ. Rev. 45:540-555.
- Minale, M. & T. Worku. 2014. Anaerobic co-digestion of sanitary wastewater and
 kitchen solid waste for biogas and fertilizer production under ambient
 temperature: waste generated from condominium house. Int. J. Environ. Sci.
 Technol. 11(2):509-516.
- Murugan, N. & P. Appavu. 2018. Investigation on low temperature biogas generation.
 Int. J. ambient energy. 39:1-3.
- Rao, P. V., S. S. Baral, R. Dey, & S. Mutnuri. 2010. Biogas generation potential by
 anaerobic digestion for sustainable energy development in India. Renew. Sust.
 Energ. Rev. 14:2086-2094.
- Sakar, S., K. Yetilmezsoy, & E. Kocak. 2009. Anaerobic digestion technology in
 poultry and livestock waste treatment a literature review. Waste Manag. Res.
 27:3-18.
- Sinbuathong, N., P. Sirirote, B. Sillapacharoenkul, J. Munakata-Marr, & S.
 Chulalaksananukul. 2012. Biogas production from two-stage anaerobic
 digestion of jatropa curcas seed cake. Energ. Source Part A. 34(22):2048-2056.
- Sutaryo, S., A. J. Ward, H. B. Møller. 2012. Thermophilic anaerobic co-digestion of
 separated solids from acidified dairy cow manure. Bioresour. Technol. 114:195 200.

| 308 | Tsigkou, K., P. Tsafrakidou, A. Kopsahelis, D. Zagklis, C. Zafiri, & M. Kornaros. |
|-----|--|
| 309 | 2020. Used disposable nappies and expired food products valorization through |
| 310 | one- & two-stage anaerobic co-digestion. Renew. Energy. 147:610-619. |
| 311 | Wilkerson, V. A., D. R. Mertens, & D. P. Casper. 1997. Prediction of Excretion of |
| 312 | Manure and Nitrogen by Holstein Dairy Cattle. J. Dairy Sci. 80:3193-3204. |
| 313 | Wei, S., H. Zhang, Z. Cai, J. Xu, J. Fang, & H. Liu. 2014. Psychrophilic anaerobic co- |
| 314 | digestion of highland barley straw with two animal manures at high altitude for |
| 315 | enhancing biogas production. Energy convers. manag. 88:40-48. |
| 316 | Yenigün, O., & B. Demirel. 2013. Ammonia inhibition in anaerobic digestion: A review. |
| 317 | Process Biochem. 48:901-911. |
| | |





- Tap water
 Water container
- 3. Measuring glass
- 4. Measuring glass holder
- 5. Teflon tube Ø 5 mm
- 6. Valve to pump and valve to tedlar gas bag
- 7. Water pump
- 8. Switch
- 9. Tedlar gas bag





330

331 Figure 2. Maximum-minimum ambient temperature during experiment



Figure 3. A. Methane yield per kg VS added.



Figure 3. B. Methane yield per digester volume per day

Table caption

Table 1. Process parameters. Values in each column followed by the same letter are not
 significantly different (p> 0.05).

| | Methane | yield | Total VFA | TAN | VS reduction | pН |
|-----------------|----------------------------|-------------------------|----------------------------|----------------------------|--------------------------|-------------------------|
| | (L/kg VS) | (L/L/d) | (mg/L) | (mg/L) | (%) | |
| R1 | 14.31±2.29 | 0.08±0.01 | 160.74 ^a ±58.95 | 137.84 ^a ±45.32 | | 6.46 ^a ±0.17 |
| R2 | 132.82±33.92 | 0.32±0.07 | 48.23 ^b ±23.73 | 178.96 ^b ±23.61 | 29.85 ^a ±6.76 | 6.84 ^b ±0.17 |
| R3 | 146.65 ^a ±42.47 | 0.31ª±0.08 | 39.19 ^b ±23.23 | 185.86 ^b ±23.68 | 28.03 ^a ±3.19 | $6.90^{b} \pm 0.28$ |
| R _{TS} | 147.13 ^a ±34.29 | 0.41 ^b ±0.07 | | | | |

2. Permintaan revisi untuk draft yang dikirim ke jurnal



Dear sutaryo sutaryo, Aldila Sempana, Cristina Lestari, Alastair Ward:

It is my pleasure to inform you that your submission to Tropical Animal Science Journal, "A Performance Comparison of Single and Two Phase Biogas Digesters Treating Dairy Cattle Manure at Tropical Ambient Temperature" had been examined by peer reviewers. Please find the comments and suggestions:

Submission URL: http://journal.ipb.ac.id/index.php/tasi/authorDashboard/submission/30343

If you decide to revise the manuscript, please give a response or rebuttal against each point which are suggested by peer reviewers. The revised document should include revision note file in table form and revised manuscript in MS Word file. Please return back the documents to the editor within 14 days via OJS, we would be glad if you submit your revised manuscript as soon as possible.

If you have any questions, please contact me.

Prof. Dr. Komang G Wiryawan

Chief Editor

FORM C1



Tropical Animal Science





Faculty of Animal Science Building, IPB University (Bogor Agricultural University) Jln. Agatis, Kampus IPB Darmaga, Bogor Indonesia 16680 Phone/Fax: +62 251 8421692 E-mail: mediapeternakan@apps.ipb.ac.id; mediapeternakan@yahoo.co.id Website: http://journal.ipb.ac.id/index.php/tasj

PAPER EVALUATION

Paper Title: Performance Comparison of Single and Two Phase Biogas Digesters Treating

Dairy Cattle Manure at Tropical Ambient Temperature

Comments (please use additional paper if more space is needed)

| No | Comments | Author's response |
|----|--|-------------------|
| Α | Reviewer I (MB1) | |
| 1 | The abstract should contain statements of introduction, objective, methods, results, and conclusion. Please revise it. | |
| 2 | Please state the novelty of the research in the Introduction before resuming the objectives. | |
| 3 | In conclusion, you should state the the prospect of your research and novelty. The conclusion should be written briefly in a single paragraph but reflects the experimental results obtained and in sync with the objectives. | |
| B | Reviewer II (MB2) | |
| 1 | This research has described the Comparison of Single and Two-Phase Biogas Digesters performance using Dairy Cattle Manure as a substrate in Tropical Ambient Temperature. Several research indicators, including methane production, Total Volatile Fatty Acid, Total Ammonia Nitrogen, etc. has been presented in this paper. The manuscript has been written in good English and also showing good scientific merit. However, I consider these several matters: | |
| 2 | The abstract should describe research design, methods, results, statistical analysis of research parameters, and conclusion, which is unsown in the manuscript. | |
| 3 | In the Introduction section, since this research wants to compare single and two-phase of biodigester equally, this section should describe the advantage of a single-phase bioreactor also. | |

| 4 | In the Material and Methods section, especially in | |
|---|---|--|
| | Experimental Set-Up, the information about R1, R2, | |
| | R3, and RTS is unclear. How many replications used | |
| | in this study? What is RTS, which is shown in several | |
| | figures and tables? There is insufficient information | |
| | about this abbreviation. | |
| 5 | In Figure 1, the resources of biogas should be shown | |
| | in this design to indicate the one and two-phase of the | |
| | biodigester. | |
| 6 | Table 1 should have a clear title, and sufficient | |
| | information about treatment initial (what is R1, R2, | |
| | R3, and RTS). The information on statistical analysis | |
| | should not be the title of the table. | |
| 7 | References | |
| | a) Please ensure that every reference cited in the | |
| | text is also present in the reference list (and | |
| | vice versa). We suggest authors to use | |
| | reference manager applications, such as | |
| | EndNote, Mendeley, etc., to prepare citations | |
| | and the list of references. | |
| | b) References should be the last 10 year | |
| | publications, with minimum 80% of journals. | |
| 8 | Please see other comments in the text | |
| 1 | | |

| 1 | Performance Comparison of Single and <u>Two-</u> Phase Biogas Digesters Treating | De | eleted: Two | |
|----|--|------|---|---|
| 2 | Dairy Cattle Manure at Tropical Ambient Temperature | | | |
| 3 | | | | |
| 4 | | | | |
| 5 | ABSTRACT | Co | mmented [A1]: Abstract should describe research design, | |
| 6 | This study examined the effect of different biogas digester configurations (single | also | o conclusion | |
| 7 | and two-phase) on methane production of dairy cattle manure (DCM) at tropical | | | |
| 8 | ambient temperature. The results showed that there was no positive effect with the | | | |
| 9 | application of a two-phase digester configuration on specific methane yield of DCM per | | | |
| 10 | kg volatile solids added. Methane production was detected in the first reactor of the | | | |
| 11 | two-phase digester configuration, and the total sum methane production of the two- | | | |
| 12 | phase digester was found to be 29.98% higher (p< 0.05) than that of the single reactor in | | | |
| 13 | terms of digester volume. Both digester configurations performed well, indicated by | | | |
| 14 | stable methane production, low volatile fatty acids, and total ammonia concentrations. | | | |
| 15 | Keywords: biogas, manure, tropical ambient temperature, two-phase digester biogas. | De | eleted: | _ |
| 16 | | | | |
| 17 | | | | |
| 18 | | | | |

| 2 | 1 |
|---|---|
| 2 | - |

INTRODUCTION

The dairy cattle industry produces large amounts of waste in the form of manure that can cause environmental pollution if not managed properly. Daily dairy cattle manure (DCM) (wet feces plus urine) excretion is 89.0; 65.9; 34.8 kg/d per 1000 kg of body weight for those that produce 29 and 14 kg/d of milk and for non-lactating dairy cows, respectively (Wilkerson *et al.*, 1997). Generally, animal waste management can take place in aerobic conditions through a composting process or by anaerobic digestion (AD) to produce biogas.

Manure management through the AD process results in numerous advantages_ 29 30 including the generation of renewable energy in the form of biogas. Biogas is the most efficient and effective among the various alternative sources of energy currently 31 available, it needs less capital investment per unit production cost compared to other 32 33 renewable energy sources, and it is available as a domestic resource in the rural areas. Therefore it is not subject to world price fluctuations (Rao et al., 2010). In addition, 34 biogas production from animal manure can create new enterprises and increases the 35 income in a rural area since it requires labor for production, collection and transport of 36 AD substrates, manufacture of technical equipment and the construction, operation, and 37 maintenance of biogas plants (Adekunle and Okolie, 2015). 38

Technically, the AD process can take places in three different temperature ranges: (1) psychrophilic (cryophilic) temperature from 10 to 20°C; (2) mesophilic temperature from 20 to 40°C; and (3) thermophilic temperature from 40 to 60°C (Burton and Turner, 2003). Based on those temperature range criteria, the AD process can be implemented at tropical ambient temperatures. Moreover, operation of AD at tropical ambient temperatures offers advantages compared to the operation of AD under

| Deleted: , t |
|--------------|
| |
| Deleted: s |
| Deleted: u |

| 48 | mesophilic or thermophilic temperatures, since AD operation at higher temperatures | Deleted: , |
|----|--|---|
| 49 | requires significant energy to maintain bioreactor temperature (Bandara et al., 2012). | |
| 50 | Among other biogas digester designs, the continuously stirred tank reactor | |
| 51 | (CSTR) design is the most commonly applied bioreactor for treating agricultural waste | |
| 52 | (Linke et al., 2015). While in operation, the process of biodegradation of organic waste | |
| 53 | can be in single or two-phases. The two-phase AD process has several advantages | Commented [A2]: Since this research want to compare single and two phase of biodigester equally. in the introduction section |
| 54 | compared to <u>a</u> single phase. These include the selection and enrichment of different | have to describe the advantage of single phase bioreactor also. |
| 55 | bacteria in each digester, increasing the stability of the process by controlling the | |
| 56 | acidification stage therefore reducing the risk of overloading and the buildup of toxic | |
| 57 | material. The first stage in the two-phase configuration can act as metabolic buffer | |
| 58 | preventing pH shock to the methanogenic microorganisms and low pH in the first stage | |
| 59 | due to a high organic loading rate favors the establishment of the acidogenic phase | Deleted: u |
| 60 | (Sinbuathong et al., 2012). Although previous studies have evaluated the AD process at | |
| 61 | ambient temperature (Minale and Worku, 2014; Wei et al., 2014; Murrugan and | |
| 62 | Appavu, 2018) and two-phase AD (Baldi et al., 2019; Tsigkou et al., 2020), to the best | Deleted: two |
| 63 | of our knowledge there has been a lack of information regarding direct comparison of | |
| 64 | single and two-phase AD of DCM at tropical ambient temperature. Therefore the aim of | Deleted: two |
| 65 | this current study was to further knowledge in this specific area. | |
| 66 | | |
| 67 | MATERIALS AND METHODS | |
| 68 | Experimental <u>Set-</u> Up | Deleted: Set |
| 69 | Evaluation of single and two-phase processes was conducted using three | Deleted: two |
| 70 | identical digesters (R1, R2, R3). The reactors were made from stainless steel, and in | Commented [A3]: Is this replication or treatment? How many replication used in this study? What is RTS which is shown in several |
| 71 | order to minimize temperature fluctuations between day and night time, all digesters | figures and table? There is insufficient information about this initial. |

| 78 | were made with double layers. The two-phase digesters consisted of reactors R1 and | Deleted: two |
|--------|--|---------------------|
| 79 | R2. Reactor 1 had a 2.1 L working volume (the minimum volume that can be applied in | |
| 80 | the reactor) and 3 d hydraulic retention (HRT), while R2 had 5.25 L working volume | |
| 81 | and 22 d HRT. Therefore in total, R1 and R2 had a 25 d HRT. R3 served as the single- | Deleted: single |
| 82 | phase bioreactor and had 5.25 L working volume and 25 d HRT. Mao et al. (2015) | |
| 83 | reported that under mesophilic conditions, an average HRT in the range of 15-30 d is | |
| 84 | required to treat waste. | |
| 85 | The experiment was started by filling R1 with 1.4 kg inoculum and 0.7 kg DCM, | Deleted: |
| 86 | R2 with 5.011 kg inoculum and 0.239 kg DCM and R3 with 5.040 kg inoculum and | |
| 87 | 0.210 kg DCM. From the second day, all digesters were fed as follows: 0.7, 0.239_{\pm} and | |
| 88 | 0.210 kg DCM for R1, R2 and R3 respectively (after first removing the same amount of | |
| 89 | digestate from a port at the base of the digesters) which continued for the following 21 d | |
| 90 | adaptation period. The digesters were fed through a tube, the outlet of which was | |
| 91 | submerged under the substrate level to avoid air ingress during the feeding process. | |
| 92 | Data were collected after this 21 d startup period. During the data collection period, R1 | |
| 93 | was fed 0.7 kg DCM. Effluent from this digester (0.239 kg) was used to feed R2, while | |
| 94 | R3 was fed 0.210 kg DCM. Digesters were kept at ambient temperature, and the | |
| 95 | experiment was run for a period of three HRT corresponding to 75 d in total. | |
| 96 | | |
| 97 | Inoculum and Substrate | |
| | | |

Inoculum in this study was sourced from the active biogas digester at the Faculty
of Animal and Agricultural Sciences, Diponegoro University. The digester treats DCM
and operates at ambient temperature. The <u>digested slurry from the digester was</u>
transferred directly to the laboratory scale digesters.

Deleted: digestate

106 Substrate was taken from dairy cows in the lactation period and was collected from the farm in the Faculty of Animal and Agricultural Sciences, Diponegoro 107 University. Manure was diluted with tap water in the ratio 1:1.5. Manure was collected 108 once per week and diluted with tap water directly and kept refrigerated. pH value, 109 volatile solids (VS) and total ammonia nitrogen (TAN) concentration in the inoculum 110 were 7.11, 7.33% and 265.18 mg/L respectively, while pH value, VS, TAN and volatile 111 fatty acids (VFA) (C2-C5) concentration of DCM were 6.77, 7.40%, 97.98 mg/L and 112 142.93 mg/L respectively. 113

114

115

Analytical Methods

Biogas from the laboratory scale bio-digesters was passed up through 0.5 L 116 infusion bottles that contained 4% NaOH solution in order to absorb CO2 using 5 ml 117 118 diameter Teflon tubing. Methane production was measured on a daily basis by 119 collecting the gas using 5 L_Tedlar gas bags using a water displacement method (Figure 1). The procedures to quantify gas production were: 1) valve to pump was in open 120 position. 2) water pump was switched on, Therefore air in the measuring glass 121 headspace was removed, and the headspace was filled up with tap water. 3) valve to 122 pump was closed. 4) water pump was switched off. 5) valve to Tedlar gas bag was 123 opened; therefore the methane in the Tedlar gas bag will move to the headspace of the 124 measuring glass. 6) gas volume was read in the measuring glass scale. When the gas 125 126 volume in the <u>Tedlar</u> gas bag exceeded the measuring glass volume, steps 1-6 were repeated. The net gas production was corrected to STP conditions. 127

Daily maximum and minimum ambient temperature was recorded using a digital hygrometer thermometer HTC-2 (Taiwan). Sample pH value was measured using a pH

| De | eted: tedlar |
|----|--------------|
| | |
| | |
| | |
| | |
| De | leted: , t |
| | |
| De | leted: |
| ٦o | latad: |
| De | ieteu. |
| De | eted: tedlar |
| | |
| De | eted: tedlar |
| ٦o | leted. |
| _ | |

5

Deleted: tedlar

| 138 | meter (Hanna® pH meter). Dry matter (DM) contents of samples were analyzed by | |
|-----|--|------|
| 139 | drying at 105°C for 7 h. Ash was determined by combusting the dried samples at 550 °C | |
| 140 | for 6 $h_{\underline{\ }}$ and VS was calculated by subtracting the ash weight from the DM | |
| 141 | (APHA,1995). TAN concentration was measured using photometric kits (HACH® | |
| 142 | USA: DOC316.53.01077) at 655 nm. VFA were determined using gas chromatography | |
| 143 | (Shimadzu GC-8). The collected data were statistically analyzed using ANOVA with | |
| 144 | 95% confidence level. Duncan's multiple range tests were used in post ANOVA | |
| 145 | analysis when differences were found to be significant (Gomez and Gomez, 2007). | |
| 146 | | |
| 147 | RESULTS | |
| 148 | Ambient Temperature Variation | |
| 149 | Average daily maximum-minimum ambient temperature throughout the | |
| 150 | experiment was 36.55°C and 20.93°C respectively (Figure 2). There was 15.63°C | |
| 151 | temperature difference between maximum temperature in day time and minimum | |
| 152 | temperature in the night time and the ambient temperature in this study therefore falls | |
| 153 | into the mesophilic category (Burton and Turner, 2033). | |
| 154 | | |
| 155 | Methane production | |
| 156 | The methane production of the three bio-digesters throughout the experiment is | |
| 157 | presented in Figure 3. The mean methane yields were 14.31 L kg/VS, 132.82 L kg/VS, | |
| 158 | and 146 L kg/VS for R1, R2 and R3 respectively Total methane yield of R1 and R2 | |
| 159 | (R _{TS}) was 147.13 L kg/VS (Table 2). A study from Amon et al. (2007) using batch | Comm |
| 160 | digesters with 60 d incubation period at 38°C showed that methane production of DCM | |
| 161 | from cows with medium milk production was 166.3 N L kg/VS while the study from | |

Commented [A4]: Where is Table 2?

162 Sutaryo et al. (2014) using continuous digesters with 20 d HRT at 35°C found that methane production of DCM was 177 L kg/VS. Both those studies were performed at 163 constant mesophilic temperature while the study presented here was performed at 164 ambient variable mesophilic temperatures, However the result of this study is similar to 165 those previous results. 166

Deleted: , h Deleted: with

167

168

Parameters in the Liquid Phase

169 Total VFA concentration and pH value of digested slurry are presented in Table 1. The mean total VFA concentration was 160.74; 48.23; 39.19 mg/L for R1, R2, and 170 171 R3, respectively. Total VFA concentration of digested slurry in R1 was significantly higher (p<0.05) than that in R2 and R3 (Table 1). TAN concentration concentrations of 172 173 digested slurry in this study were 137.85; 178.96; 185.86 mg/L for R1, R2, and R3, 174 respectively (Table 2).

Volatile solid reductions in this study were 29.85 and 28.03% for R2 and R3 175 respectively. Study from Bhattacharya et al. (1996) found a VS reduction of 26% and 176 177 30% for conventional and two-phase digester respectively, treating sludges from conventional activated sludge treatment plants and maintained at 35°C. Meanwhile, a 178 179 study from Sutaryo et al. (2012) found a VS reduction in range of 27-35% for a reactor treating DCM with different TS concentrations. Therefore the result of this study is in 180 accordance with the result of the previous study. 181

- 182
- 183

Commented [A5]: Where is Table 2?

DISCUSSION

Ambient Temperature Variation

This study was performed in July-September, and in Indonesia that period is considered to be in the dry season. A large variation temperature in AD operation in the course of this study therefore has an adverse impact on the microorganism activity. Sakar *et al.* (2009) reported that the AD process is carried out by a <u>balanced prime</u> population of various microorganisms. These microorganisms are very sensitive to environmental condition changes including temperature.

194

186

187

195

Methane production

There was no significant effect (p>0.05) of the application of a two-phase bio-196 digester on specific methane yield in terms of kg VS of substrate added when compared 197 198 to that from the single digester configuration (Table 1). However, methane production of RTS was significantly higher (p<0.05) than that in R3 in term of L/L digester volume 199 (methane production/volume active). No significant effect (p>0.05) of the application of 200 the two-stage digester than single digester on specific methane yield in this study can 201 be due to anaerobic microorganisms activities in both reactors configuration operation 202 efficiently. This study used digested slurry from an active digester that operated at a 203 tropical ambient temperature, the same condition used in this study. This fact, along 204 with the three weeks adaptation period, contributed to the efficient microorganism's 205 activity in both reactor configurations in this study even though there was a large 206 temperature difference between day and night time. A study by Chae et al. (2008) found 207 that using batch digesters and treating swine manure, the methane production at 30 and 208 209 35°C were quite similar, but it was higher by more than 13-17% than that at 25°C.

Deleted: prime balanced

Deleted: two

Temperature shocks caused a reduction in the methane production rate compared to that of the control, but it recovered rapidly. Once adapted, no significant effect on the methane production was observed between the control and the temperature shock biodigester. This fact therefore indicates that, even though methanogenic archaea are quite sensitive to temperature shock they have considerable ability to adapt to temperature changes (Chae *et al.*, 2008).

Methane production in term of digester volume of RTS was 29.98% higher than 218 that in R3. The positive effect (p<0.05) of the application of two phase digestion on the 219 methane production compared to that in the single phase reactor can be attributed to a 220 221 shorter HRT period in R1 and R2 than that in R3, therefore the amount of substrate added to R1 and R2 was higher than that in R3. Since the amount of substrate added to 222 R2 (0.239 kg) was higher than that in R3 (0.210 kg) and in the same time the active 223 224 volume in both digester configurations was equal (5.25 L) therefore methane production in term of digester volume R2 was higher than that in R3. In fact methane production in 225 RTS was methane yield in R1 and in R2. In this present study, HRT in R1, R2 and R3 226 were 3 d, 22 d and 25 d respectively. Bhattacharya et al. (1996) reported that one of the 227 advantages of phase separation is the ability to handle a higher organic loading rate than 228 that in a single reactor. A similar study from Tsigkou et al. (2020) found the same 229 230 phenomenon, in that the application of a two-stage digester treating co-digestion of used disposable nappies and expired food product at 60:40 (v/v) ratio, working at mesophilic 231 condition (37±0.5°C) and 15 d HRT the energy production was 18.5% higher than that 232 in the single reactor. 233

- 234
- 235

Parameters in the Liquid Phase

236 During bioconversion of organic matter in AD system there are four steps, namely hydrolysis, acidogenesis, acetogenesis and methanogenesis. In a two stage 237 digester configuration, the first digester serves as the acidogenic phase (Sinbuatong et 238 al., 2012), therefore the VFA concentration will be higher than that in the second 239 digester. A higher total VFA concentration in R1 than that on other reactor in this study 240 is in accordance with Baldi et al. (2019) who found that total VFA concentration of 241 digested slurry in a fermentative digester was significantly higher than that of digested 242 slurry from methanogenic digester. 243

The higher VFA concentration of R1-digested slurry gave consequences on the lower pH value (p<0.05) than that in R2 and R3-digested slurry. The mean pH values of digested slurry in this recent study were 6.46; 6.84 and 6.89 for R1, R2 and R3 respectively. The pH value of R2 and R3 in this recent study was in the range of a stable AD process. Mao *et al.* (2015) reported that the ideal pH value for AD process is in the range of 6.8 to 7.4.

Ammonia is one of the essential nutrients for the growth of microorganisms, 250 however it can inhibit the AD process if it is available at high concentrations (Yenigün 251 and Demirel, 2013). Under mesophilic conditions (35°C), the TAN inhibitory threshold 252 was in the concentrations of around 1700-1800 mg L-1 for unacclimated inoculum 253 (Yenigün and Demirel, 2013). TAN concentration of digested slurry in R1 was 254 significantly lower (p<0.05) than that in R2 and R3. This fact can be attributed to a 255 shorter HRT in R1 than that in R2 and R3 therefore microorganisms in R2 and R3 can 256 257 degrade more protein in the substrate, subsequently producing more ammonia. However TAN concentrations of digested slurry from all digester in this study were below the 258 inhibitory level as reported by Yenigün and Demirel (2013). 259

| 260 | There was no significant effect ($p>0.05$) of the application two stage compared | |
|-----|--|--|
| 261 | to single stage digesters on the VS reduction. No significant effect of phase separation | |
| 262 | on volatile solid reduction in this study suggests that microorganisms in both reactor | |
| 263 | configurations can work well. | |
| 264 | | |
| 265 | CONCLUSION | |
| 266 | It has been demonstrated that the application of a two-phase digester treating | |
| 267 | DCM working at tropical ambient temperature significantly increased methane | |
| 268 | production by 29.98% compare to the single stage reactor in term of digester volume. | |
| 269 | However, no significant effect of this digester configuration on specific methane yield | |
| 270 | in terms of VS. Both digester configurations can run properly with stable methane | |
| 271 | production, low VFA and TAN concentrations. Therefore the two-phase digester | |
| 272 | configuration in tropical ambient temperature can be applied to increase methane | |
| 273 | production in term of digester volume. | |
| 274 | | |
| 275 | CONFLICT OF INTEREST | |
| 276 | We certify that there is no conflict of interest with any financial, personal, or | |
| 277 | other relationships with other people or organization related to the material discussed in | |
| 278 | the manuscript. | |
| 279 | | |
| 280 | ACKNOWLEDGEMENT | |
| 281 | The authors would like to thank Diponegoro University (grant number: | |
| 282 | 109/UN7.5.5/PP/2018) for financing this study. | |
| 283 | | |

| 285 | Adekunle, K. F. & J. A. Okolie. 2015. A Review of Biochemical Process of Anaerobic |
|---|---|
| 286 | Digestion. Adv. Biosci. Biotechnol. 6:205-212. |
| 287 | Amon, T., B. Amon, V. Kryvoruchko, W. Zollitsch, K. Mayer, & L. Gruber. 2007. |
| 288 | Biogas production from maize and dairy cattle manure-Influence of biomass |
| 289 | composition on the methane yield. Agric Ecosyst Environ. 118:173-182. |
| 290 | APHA, 1995. Standard Methods for Examination of Water and Waste Water, 19th ed. |
| 291 | American Public Health Association, Washington, DC. |
| 292 | Bhattacharya, S. K., R. L. Madura, D. A. Walling, & J. B. Farrell. 1996. Volatile |
| 293 | solids reduction in two-phase and conventional anaerobic sludge digestion. |
| 294 | Water Res. 30(5):1041-1048. |
| | |
| 295 | Bandara, W. M. K. R. T. W., T. Kindaichi, H. Satoh, M. Sasakawa, Y. Nakahara, |
| 295 296 | Bandara, W. M. K. R. T. W., T. Kindaichi, H. Satoh, M. Sasakawa, Y. Nakahara,M. Takahashi, & S. Okabe. 2012. Anaerobic treatmentofmunicipal wastewater |
| 295 296 297 | Bandara, W. M. K. R. T. W., T. Kindaichi, H. Satoh, M. Sasakawa, Y. Nakahara, M. Takahashi, & S. Okabe. 2012. Anaerobic treatmentofmunicipal wastewater at ambient temperature: Analysis of archaeal community structure and recovery |
| 295 296 297 298 | Bandara, W. M. K. R. T. W., T. Kindaichi, H. Satoh, M. Sasakawa, Y. Nakahara, M. Takahashi, & S. Okabe. 2012. Anaerobic treatmentofmunicipal wastewater at ambient temperature: Analysis of archaeal community structure and recovery of dissolved methane. Water Res. 46:5756-5764. |
| 295 296 297 298 299 | Bandara, W. M. K. R. T. W., T. Kindaichi, H. Satoh, M. Sasakawa, Y. Nakahara, M. Takahashi, & S. Okabe. 2012. Anaerobic treatmentofmunicipal wastewater at ambient temperature: Analysis of archaeal community structure and recovery of dissolved methane. Water Res. 46:5756-5764. Baldi, F., L. Pecorini, & R. Iannelli. 2019. Comparison of single-stage and two-stage |
| 295 296 297 298 299 300 | Bandara, W. M. K. R. T. W., T. Kindaichi, H. Satoh, M. Sasakawa, Y. Nakahara, M. Takahashi, & S. Okabe. 2012. Anaerobic treatmentofmunicipal wastewater at ambient temperature: Analysis of archaeal community structure and recovery of dissolved methane. Water Res. 46:5756-5764. Baldi, F., L. Pecorini, & R. Iannelli. 2019. Comparison of single-stage and two-stage anaerobic co-digestion of food waste and activated sludge for hydrogen and |
| 295 296 297 298 299 300 | Bandara, W. M. K. R. T. W., T. Kindaichi, H. Satoh, M. Sasakawa, Y. Nakahara, M. Takahashi, & S. Okabe. 2012. Anaerobic treatmentofmunicipal wastewater at ambient temperature: Analysis of archaeal community structure and recovery of dissolved methane. Water Res. 46:5756-5764. Baldi, F., L. Pecorini, & R. Iannelli. 2019. Comparison of single-stage and two-stage anaerobic co-digestion of food waste and activated sludge for hydrogen and methane production. Renew Energy. 43:1755-1765. |
| 295 296 297 298 299 300 301 302 | Bandara, W. M. K. R. T. W., T. Kindaichi, H. Satoh, M. Sasakawa, Y. Nakahara, M. Takahashi, & S. Okabe. 2012. Anaerobic treatmentofmunicipal wastewater at ambient temperature: Analysis of archaeal community structure and recovery of dissolved methane. Water Res. 46:5756-5764. Baldi, F., L. Pecorini, & R. Iannelli. 2019. Comparison of single-stage and two-stage anaerobic co-digestion of food waste and activated sludge for hydrogen and methane production. Renew Energy. 43:1755-1765. Burton, C.H. & Turner, C., 2003. Anaerobic treatment options for animal manures. |
| 295 296 297 298 299 300 301 302 303 | Bandara, W. M. K. R. T. W., T. Kindaichi, H. Satoh, M. Sasakawa, Y. Nakahara, M. Takahashi, & S. Okabe. 2012. Anaerobic treatmentofmunicipal wastewater at ambient temperature: Analysis of archaeal community structure and recovery of dissolved methane. Water Res. 46:5756-5764. Baldi, F., L. Pecorini, & R. Iannelli. 2019. Comparison of single-stage and two-stage anaerobic co-digestion of food waste and activated sludge for hydrogen and methane production. Renew Energy. 43:1755-1765. Burton, C.H. & Turner, C., 2003. Anaerobic treatment options for animal manures. In: Manure Management – Treatment Strategies for Sustainable Agriculture, 2nd |

REFERENCES

284

305 Measure project, MATRESA, Wrest Park, Silsoe, Bedford, UK.
| 307 | temperature and temperatureshock on the biogas yields from the mesophilic |
|-----|---|
| 308 | anaerobic digestion of swine manure. Bioresour. Technol. 99:1-6. |
| 309 | Gomez, K. A., & A. A. Gomez. 2007. Prosedur statistik untuk penelitian pertanian. |
| 310 | Translated by Sjamsuddin, E., & J. S. Baharsjah. UI Press, Jakarta. |
| 311 | Linke, B., A. Rodríguez-Abalde, C. Jost, & A. Krieg. 2015. Performance of a novel |
| 312 | two-phase continuously fed leach bed reactor for demand-based biogas |
| 313 | production from maize silage. Bioresour. Technol. 177:34-40. |
| 314 | Mao, C., Y. Feng, X. Wang, & G. Ren. 2015. Review on research achievements of |
| 315 | biogas from anaerobic digestion. Renew. Sust. Energ. Rev. 45:540-555. |
| 316 | Minale, M. & T. Worku. 2014. Anaerobic co-digestion of sanitary wastewater and |
| 317 | kitchen solid waste for biogas and fertilizer production under ambient |
| 318 | temperature: waste generated from condominium house. Int. J. Environ. Sci. |
| 319 | Technol. 11(2):509-516. |

Chae, K. J., S. K. Am Jang, L. Yim, & S. Kim. 2008. The effects of digestion

- Murugan, N. & P. Appavu. 2018. Investigation on low temperature biogas generation.
 Int. J. ambient energy. 39:1-3.
- 322 Rao, P. V., S. S. Baral, R. Dey, & S. Mutnuri. 2010. Biogas generation potential by
- anaerobic digestion for sustainable energy development in India. Renew. Sust.
 Energ. Rev. 14:2086-2094.
- 325 Sakar, S., K. Yetilmezsoy, & E. Kocak. 2009. Anaerobic digestion technology in
 326 poultry and livestock waste treatment a literature review. Waste Manag. Res.
- 327 27:3-18.

| 328 | Sinbuathong, N., P. Sirirote, B. Sillapacharoenkul, J. Munakata-Marr, & S. |
|-----|---|
| 329 | Chulalaksananukul. 2012. Biogas production from two-stage anaerobic |
| 330 | digestion of jatropa curcas seed cake. Energ. Source Part A. 34(22):2048-2056. |
| 331 | Sutaryo, S., A. J. Ward, H. B. Møller. 2012. Thermophilic anaerobic co-digestion of |
| 332 | separated solids from acidified dairy cow manure. Bioresour. Technol. 114:195- |
| 333 | 200. |
| 334 | Tsigkou, K., P. Tsafrakidou, A. Kopsahelis, D. Zagklis, C. Zafiri, & M. Kornaros. |
| 335 | 2020. Used disposable nappies and expired food products valorization through |
| 336 | one- & two-stage anaerobic co-digestion. Renew. Energy. 147:610-619. |
| 337 | Wilkerson, V. A., D. R. Mertens, & D. P. Casper. 1997. Prediction of Excretion of |
| 338 | Manure and Nitrogen by Holstein Dairy Cattle. J. Dairy Sci. 80:3193-3204. |
| 339 | Wei, S., H. Zhang, Z. Cai, J. Xu, J. Fang, & H. Liu. 2014. Psychrophilic anaerobic |
| 340 | co-digestion of highland barley straw with two animal manures at high altitude |
| 341 | for enhancing biogas production. Energy convers. manag. 88:40-48. |
| 342 | Yenigün, O., & B. Demirel. 2013. Ammonia inhibition in anaerobic digestion: A |
| 343 | review. Process Biochem. 48:901-911. |



Figure 2. Maximum-minimum ambient temperature during experiment 357





360 Figure 3. A. Methane yield per kg VS added.







363 Figure 3. B. Methane yield per digester volume per day

366 Table caption

Table 1. Process parameters. Values in each column followed by the same letter are not significantly different (p> 0.05).

| Significantly different (p> 0.05). Methane yield Total VFA TAN VS reduction Sufficient information about treatment initial (will and RTS). The information of statistical analysis state of the table. (L/kg VS) (L/L/d) (mg/L) (mg/L) (%) R1 14.31±2.29 0.08±0.01 160.74 ^a ±58.95 137.84 ^a ±45.32 6.46 ^a ±0.17 R2 132.82±33.92 0.32±0.07 48.23 ^b ±23.73 178.96 ^b ±23.61 29.85 ^a ±6.76 6.84 ^b ±0.17 | significantly Metha (L/kg VS) | | lifferent (p>0.0 e yield | p>0.05). | | | Ca | ommented [A7]: The Table should have clear tittle, and |
|--|---|--------------------|-----------------------------|----------------------------------|----------------------------|--------------------------|---------------------|--|
| $\begin{tabular}{ c c c c c c c c c c c c c c c c c c c$ | Metha (L/kg VS) | | e yield | Tetal VEA | | | | |
| (L/kg VS) (L/L/d) (mg/L) (mg/L) (%) R1 14.31±2.29 0.08±0.01 160.74 ^a ±58.95 137.84 ^a ±45.32 6.46 ^a ±0.17 R2 132.82±33.92 0.32±0.07 48.23 ^b ±23.73 178.96 ^b ±23.61 29.85 ^a ±6.76 6.84 ^b ±0.17 | (L/kg VS) | | • | TOTAL VEA | TAN | VS reduction | su an | fficient information about treatment initial (what is R1, R2, R3, d RTS). The information of statistical analysis should not to be a |
| R1 14.31 ± 2.29 0.08 ± 0.01 $160.74^{a}\pm58.95$ $137.84^{a}\pm45.32$ $6.46^{a}\pm0.17$ R2 132.82 ± 33.92 0.32 ± 0.07 $48.23^{b}\pm23.73$ $178.96^{b}\pm23.61$ $29.85^{a}\pm6.76$ $6.84^{b}\pm0.17$ | $(\mathbf{L},\mathbf{R},\mathbf{S},\mathbf{D})$ | | (L/L/d) | /d) (mg/L) | (mg/L) | (%) | tit | le of the table. |
| R1 14.31 ± 2.29 0.08 ± 0.01 $160.74^{a}\pm58.95$ $137.84^{a}\pm45.32$ $6.46^{a}\pm0.17$ R2 132.82 ± 33.92 0.32 ± 0.07 $48.23^{b}\pm23.73$ $178.96^{b}\pm23.61$ $29.85^{a}\pm6.76$ $6.84^{b}\pm0.17$ | | | (12,12,4) | (iiig, 1) | (1116) (2) | (/0) | | |
| R2 132.82 \pm 33.92 0.32 \pm 0.07 48.23 ^b \pm 23.73 178.96 ^b \pm 23.61 29.85 ^a \pm 6.76 6.84 ^b \pm 0.17 | 14.31±2.29 | R1 | 0.08 ± 0.01 | ±0.01 160.74 ^a ±58.95 | 137.84 ^a ±45.32 | | 6.46 ^a | ±0.17 |
| | 132.82+33.92 | R2 1 | 0.32+0.07 | $48.23^{b}+23.73$ | 178.96 ^b +23.61 | 29.85 ^a +6.76 | 6.84 ^b - | +0.17 |
| | 102.02_00.01 | 112 1 | 0.52_0.07 | 10.23 _23.73 | 170.90 _23.01 | 27.00 20.10 | 0.01 | |
| R3 $146.65^{a}\pm42.47$ $0.31^{a}\pm0.08$ $39.19^{b}\pm23.23$ $185.86^{b}\pm23.68$ $28.03^{a}\pm3.19$ $6.90^{b}\pm0.28$ | $146.65^{a}\pm42.47$ | R3 14 | $0.31^{a}\pm0.08$ | ±0.08 39.19 ^b ±23.23 | $185.86^{b} \pm 23.68$ | $28.03^{a}\pm3.19$ | 6.90 ^b | ±0.28 |
| $\mathbf{R}_{TS} = 147 \cdot 13^{a} + 34 \cdot 29 = 0 \cdot 41^{b} + 0 \cdot 07$ | $147 13^{a}+34 20$ | R _{TE} 14 | $0.41^{b}+0.07$ | 2+0.07 | | | | |
| | 147.15 ±54.2 | 113 1- | 0.41 ±0.07 | -0.07 | | | | |

3. Perbaikan draft publikasi dari penulis

Surat pengantar, respon penulis dan draft publikasi versi revisi

Dear Prof. Dr. Komang G. Wiryawan The Editor, Tropical Animal Science Journal, 17th May 2020

Subject: Resubmission of manuscript titled 'Performance Comparison of Single and Two-Phase Biogas Digester Treating Dairy Cattle Manure at Tropical Ambient Temperature' (manuscript number: TASJ_30343)

- authored by Sutaryo Sutaryo, A. N. Sempana, C. M. S. Lestari, Alastair James Ward

We herewith resubmit our paper with the title **Performance Comparison of Single and Two-Phase Biogas Digesters Treating Dairy Cattle Manure at Tropical Ambient Temperature**. The manuscript is an original article based on the experiments carried out during 2018 at Faculty Animal and Agricultural Sciences, Diponegoro University.

Thank you for the opportunity you provide us to resubmit our manuscript. The authors greatly appreciate the constructive comments given by both the reviewers. In the attached new version of the manuscript (revised manuscript), changes in response to the reviewers' comments have been highlighted using blue text.

I thank you for your time and consideration, and look forward to hearing from you.

Thank you and best regards,

On behalf of all the authors,

Sutaryo Sutaryo Dept. of Animal Science Faculty Animal and Agricultural Sciences Diponegoro University Kampus Tembalang 50275 Email: <u>soeta@lecturer.undip.ac.id</u>

FORM C1



Tropical Animal Science





Faculty of Animal Science Building, IPB University (Bogor Agricultural University) Jln. Agatis, Kampus IPB Darmaga, Bogor Indonesia 16680 Phone/Fax: +62 251 8421692 E-mail: mediapeternakan@apps.ipb.ac.id; mediapeternakan@yahoo.co.id Website: http://journal.ipb.ac.id/index.php/tasj

PAPER EVALUATION

Paper Title: Performance Comparison of Single and Two Phase Biogas Digester Treating Dairy Cattle Manure at Tropical Ambient Temperature

| No | Comments | Author's response |
|----|---|---|
| A | Reviewer I (MB1) | The authors tanks for the valuable and constructive comments given by reviewers. The manuscript has been revised carefully. All comments have been addressed by either accepting them or giving more information and discussion and those are highlighted with dark blue colour. |
| 1 | The abstract should contain statements of introduction, objective, methods, results, and conclusion. | Abstract has been revised according reviewer suggestion: |
| | Please revise it. | The biodegradation process of organic waste in anaerobic digestion can be in single or two-phase bio- reactor. This study examined the effect of different biogas digester configurations (single and two-phase) on methane production of dairy cattle manure (DCM) at tropical ambient temperature. Three identical reactors were used in this study (R1, R2, and R3). The two-phase digesters consisted of reactors R1 and R2. R1 had a 2.1 L working volume and 3 d hydraulic retention time (HRT), while R2 had 5.25 L working volume and 22 d HRT (R1 and R2 had a 25 d HRT). The digested slurry of R1 was used to feed R2. R3 served as the single-phase digester and had 5.25 L working volume and 25 d HRT. Methane production were 14.31, 132.82, and 146 L/kg VS for R1, R2 and R3 respectively. The results showed that there was no positive effect (p>0.05) with the application of a two-phase digester configuration on |

Comments (please use additional paper if more space is needed)

| | | specific methane yield of DCM per kg volatile solids added than that in the single-reactor. Methane production was detected in the first reactor of the two- phase digester configuration and the total sum methane production of the two-phase digester was found to be 29.98% higher (p<0.05) than that of the single reactor in terms of digester volume (0.41 VS 0.31 L/L/d). Both digester configurations performed well, indicated by stable methane production, low volatile fatty acids, and total ammonia concentrations. The two-phase bio- digester configuration can increase significantly methane production in terms of digester volume. |
|---|---|---|
| 2 | Please state the novelty of the research in the | This information has been written by the author in the introduction section. |
| | Introduction before resuming the objectives. | There has been a lack of information regarding direct comparison of single and two-phase AD of DCM at tropical ambient temperature |
| 3 | In conclusion, you should state the the prospect of | Conclusion has been revised according reviewer suggestion. |
| D | your research and novelty. The conclusion should be written briefly in a single paragraph but reflects the experimental results obtained and in sync with the objectives. | It has been demonstrated that the application of a two- phase digester treating DCM working at a tropical ambient temperature significantly increased methane production by 29.98% compared to the single stage reactor in terms of digester volume. However, no significant effect of this digester configuration on specific methane yield in terms of VS. Both digester configurations can run properly with stable methane production, low VFA, and TAN concentrations. Therefore the two-phase digester configuration in tropical ambient temperature can be applied to increase methane production in terms of digester volume. However, to be implemented on an industrial scale, further study is needed related to the addition of infrastructure to the two-phase digester rather than the single reactor. |
| B | Reviewer II (MB2) | |
| 1 | This research has described the Comparison of Single and Two-Phase Biogas Digesters performance using Dairy Cattle Manure as a substrate in Tropical Ambient Temperature. | |

| | Several research indicators, including methane production, Total Volatile Fatty Acid, Total Ammonia Nitrogen, etc. has been presented in this paper. The manuscript has been written in good English and also showing good scientific merit. However, I consider these several matters: | |
|---|--|--|
| 2 | The abstract should describe research design, methods, results, statistical analysis of research parameters, and conclusion, which is unsown in the manuscript. | Abstract has been revised according reviewer suggestion: The biodegradation process of organic waste in anaerobic digestion can be in single or two-phase bio- reactor. This study examined the effect of different biogas digester configurations (single and two-phase) on methane production of dairy cattle manure (DCM) at tropical ambient temperature. Three identical reactors were used in this study (R1, R2, and R3). The two-phase digesters consisted of reactors R1 and R2. R1 had a 2.1 L working volume and 3 d hydraulic retention time (HRT), while R2 had 5.25 L working volume and 22 d HRT (R1 and R2 had a 25 d HRT). The digested slurry of R1 was used to feed R2. R3 served as the single-phase digester and had 5.25 L working volume and 25 d HRT. Methane production were 14.31, 132.82, and 146 L/kg VS for R1, R2 and R3 respectively. The results showed that there was no positive effect (p>0.05) with the application of a two-phase digester configuration on specific methane yield of DCM per kg volatile solids added than that in the single-reactor. Methane production was detected in the first reactor of the two- phase digester configuration and the total sum methane production of the two-phase digester was found to be 29.98% higher (p<0.05) than that of the single reactor in terms of digester volume (0.41 VS 0.31 L/L/d). Both digester configurations performed well, indicated by stable methane production, low volatile fatty acids, and total ammonia concentrations. The two-phase bio- digester configuration can increase significantly methane production in terms of digester volume. |

| 3 | In the Introduction section, since this research wants to compare single and two- phase of biodigester equally, this section should describe the advantage of a single-phase bioreactor also. | The advantage of a single-phase bioreactor has been added in the introduction section. On the other hand, single-phase bio-digester has also advantageous as it is a simple and straightforward operation and for easier degradable substrate such as fruit and vegetables waste single-phase process could be the preferred rather than two-phase reactor (Ganesh <i>et al.</i> , 2014). |
|---|--|---|
| 4 | In the Material and Methods section, especially in Experimental Set-Up, the information about R1, R2, R3, and RTS is unclear. How many replications used in this study? What is RTS, which is shown in several figures and tables? There is insufficient information about this abbreviation. | Thank you very much for the corrections. R1, R2 and R3 is the name of digester, this information has been added. Evaluation of single and two-phase processes was conducted using three identical digesters, namely R1, R2, R3. R_{TS} is total sum methane production of R1 and R2. This information is in L153-154 P 8. Total methane yield of R1 and R2 (R_{TS}). The replication in this study is the data collection period for three hydraulic retention time (HRT). It is common in biogas study therefore more than 95% of inoculum has been replaced by substrate rather than using replication in the number of the digester. This information is in materials and methods section L102-103 P5. Digesters were kept at ambient temperature, and the experiment was run for a period of three HRT corresponding to 75 d in total. |
| 5 | In Figure 1, the resources of biogas should be shown in this design to indicate the one and two-phase of the biodigester. | Methane production from both digesters configuration is collected using a Tedlar gas bag. When measuring the gas volume, the Tedlar gas bag is removed from the digester series after the valve is closed first. Then the gas bag is connected to the apparatus. Thus the circuit is only used to measure the production of gas in the gas bag. Therefore, it is not connected to the gas resource in all time. |
| 6 | Table 1 should have a clear title, and sufficient information about treatment initial (what is R1, R2, R3, and RTS). The information on statistical analysis should not be the title of the table. | Thank you very much for the correction. Table 1 has been revised according reviewer suggestion. |

| 7 | Refere | nces | - Thank you for the reviewer suggestion. Reference |
|---|------------------|--|---|
| | c) | Please ensure that every reference cited in the text is also present in the reference list (and vice versa). We suggest authors to use reference manager | has been check. Some old references have been replaced with new ones. 1. Amon, T., B. Amon, V. Kryvoruchko, W. Zollitsch, K. Mayer, & L. Gruber. 2007. Biogas production from maize and dairy cattle manure-Influence of biomass composition on the methane yield. <i>Agric Ecosyst Environ</i>. 118:173-182. Replaced by: |
| | | as EndNote, Mendeley, etc., to prepare citations and the list of references. | Yamashiro, & K. Umetsu. 2013. The combined effect of cefazolin and oxytertracycline on biogas production from thermophilic anaerobic digestion of dairy manure. Bioresource Biotechnol. 133:23-30. |
| | d) | References should be the last 10 year publications, with minimum 80% of journals. | 2. Wilkerson, V. A., D. R. Mertens, & D. P. Casper. 1997. Prediction of Excretion of Manure and Nitrogen by Holstein Dairy Cattle. J. Dairy Sci. 80:3193-3204. Replaced by: |
| | | | 3. Bhattacharya, S. K., R. L. Madura, D. A. Walling, & J. B. Farrell. 1996. Volatile solids reduction in two-phase and conventional anaerobic sludge digestion. Water Res. 30(5):1041-1048. Replaced by: |
| | | | Brown, D. & Y. Li. 2013. Solid state anaerobic co- digestion of yard waste and food waste for biogas production. Bioresour. Technol. 127:275-280. |
| | | | 4. Sakar, S., K. Yetilmezsoy, & E. Kocak. 2009. Anaerobic digestion technology in poultry and livestock waste treatment – a literature review. Waste Manag. Res. 27:3-18. Replaced by: |
| | | | Mao, C., Y. Feng, X. Wang, & G. Ren. 2015. Review on research achievements of biogas from anaerobic digestion. Renew. Sust. Energ. Rev. 45:540-555. |
| 8 | Please in the | see other comments text | Thank you very much for the valuable comments. The manuscript has been revised according reviewer comments. |

| 1 | Performance Comparison of Single and Two-Phase Biogas Digester Treating Dairy |
|----|---|
| 2 | Cattle Manure at Tropical Ambient Temperature |
| 3 | |
| 4 | S. Sutaryo ^a *, A. N. Sempana ^a , C. M. S. Lestari ^a , A. J. Ward ^b |
| 5 | |
| 6 | ^a Department of Animal Science, Faculty of Animal and Agricultural Sciences, |
| _ | |
| 7 | Diponegoro University, Semarang, Indonesia |
| 0 | ^b Department of Engineering Engulty of Science and Technology, Aerbug University |
| ŏ | Department of Engineering, Faculty of Science and Technology, Aarnus Oniversity, |
| ٩ | Aarhus Denmark |
| 5 | Admus, Denmark |
| 10 | *Corresponding author: soeta@lecturer.undip.ac.id: sutaryoundip@yahoo.com |
| | |

ABSTRACT

The biodegradation process of organic waste in anaerobic digestion can be in 12 single or two-phase bio-reactor. This study examined the effect of different biogas 13 digester configurations (single and two-phase) on methane production of dairy cattle 14 manure (DCM) at tropical ambient temperature. Three identical reactors were used in this 15 study (R1, R2, and R3). The two-phase digesters consisted of reactors R1 and R2. R1 had 16 a 2.1 L working volume and 3 d hydraulic retention time (HRT), while R2 had 5.25 L 17 18 working volume and 22 d HRT (R1 and R2 had a 25 d HRT). The digested slurry of R1 was used to feed R2. R3 served as the single-phase digester and had 5.25 L working 19 volume and 25 d HRT. Methane production were 14.31, 132.82, and 146 L/kg VS for R1, 20 21 R2 and R3 respectively. The results showed that there was no positive effect (p>0.05) with the application of a two-phase digester configuration on specific methane yield of 22 DCM per kg volatile solids added than that in the single-reactor. Methane production was 23 detected in the first reactor of the two-phase digester configuration and the total sum 24 25 methane production of the two-phase digester was found to be 29.98% higher (p < 0.05) 26 than that of the single reactor in terms of digester volume (0.41 VS 0.31 L/L/d). Both 27 digester configurations performed well, indicated by stable methane production, low volatile fatty acids, and total ammonia concentrations. The two-phase bio-digester 28 29 configuration can increase significantly methane production in terms of digester volume. Keywords: biogas, manure, tropical ambient temperature, two-phase digester biogas. 30

- 31
- 32
- 33

INTRODUCTION

The dairy cattle industry produces large amounts of waste in the form of manure that can cause environmental pollution if not managed properly. Daily dairy cattle manure (DCM) (wet feces plus urine) excretion is 2226.5 kg/year per 610 kg of body weight (Noorollahi *et al.*, 2015). Generally, animal waste management can take place in aerobic conditions through a composting process or by anaerobic digestion (AD) to produce biogas.

Manure management through the AD process results in numerous advantages, 41 including the generation of renewable energy in the form of biogas. Biogas is the most 42 efficient and effective among the various alternative sources of energy currently 43 44 available, it needs less capital investment per unit production cost compared to other renewable energy sources, and it is available as a domestic resource in the rural areas. 45 Therefore it is not subject to world price fluctuations (Rao et al., 2010). In addition, biogas 46 production from animal manure can create new enterprises and increases the income in a 47 rural area since it requires labor for production, collection and transport of AD substrates, 48 49 manufacture of technical equipment and the construction, operation and maintenance of 50 biogas plants (Adekunle and Okolie, 2015).

Technically, the AD process can take places in three different temperature ranges: (1) psychrophilic (cryophilic) temperature from 10 to 20°C; (2) mesophilic temperature from 20 to 40°C; and (3) thermophilic temperature from 40 to 60°C (Burton and Turner, 2003). Based on those temperature range criteria, the AD process can be implemented at tropical ambient temperatures. Moreover, operation of AD at tropical ambient temperatures offers advantages compared to the operation of AD under mesophilic or

thermophilic temperatures since AD operation at higher temperatures requires significant energy to maintain bioreactor temperature (Bandara *et al.*, 2012).

58

Among other biogas digester designs, the continuously stirred tank reactor 59 (CSTR) design is the most commonly applied bioreactor for treating agricultural waste 60 61 (Linke et al., 2015). While in operation, the process of biodegradation of organic waste can be in single or two-phases. The two-phase AD process has several advantages 62 compared to a single phase. These include the selection and enrichment of different 63 64 bacteria in each digester, increasing the stability of the process by controlling the acidification stage therefore reducing the risk of overloading and the buildup of toxic 65 material. The first stage in the two-phase configuration can act as metabolic buffer 66 preventing pH shock to the methanogenic microorganisms and low pH in the first stage 67 due to a high organic loading rate favors the establishment of the acidogenic phase 68 (Sinbuathong et al., 2012). On the other hand, single-phase bio-digester has also 69 advantageous as it is a simple and straightforward operation and for easier degradable 70 71 substrate such as fruit and vegetables waste single-phase process could be the preferred 72 rather than two-phase reactor (Ganesh et al., 2014). Although previous studies have 73 evaluated the AD process at ambient temperature (Minale and Worku, 2014; Wei et al., 2014; Murrugan and Appavu, 2018) and two-phase AD (Baldi et al., 2019; Tsigkou et 74 75 al., 2020), to the best of our knowledge there has been a lack of information regarding direct comparison of single and two-phase AD of DCM at tropical ambient temperature. 76 77 Therefore the aim of this current study was to further knowledge in this specific area.

- 78
- 79

MATERIALS AND METHODS

80

Experimental Set-Up

Evaluation of single and two-phase processes was conducted using three identical 81 82 digesters, namely R1, R2, R3. The reactors were made from stainless steel, and in order to minimize temperature fluctuations between day and night time, all digesters were made 83 with double layers. The two-phase digesters consisted of reactors R1 and R2. Reactor 1 84 85 had a 2.1 L working volume (the minimum volume that can be applied in the reactor) and 3 d hydraulic retention (HRT), while R2 had 5.25 L working volume and 22 d HRT. 86 Therefore in total, R1 and R2 had a 25 d HRT. R3 served as the single-phase bioreactor 87 88 and had 5.25 L working volume and 25 d HRT. Mao et al. (2015) reported that under mesophilic conditions, an average HRT in the range of 15-30 d is required to treat waste. 89 The experiment was started by filling R1 with 1.4 kg inoculum and 0.7 kg DCM, 90 91 R2 with 5.011 kg inoculum, and 0.239 kg DCM and R3 with 5.040 kg inoculum and 0.210 kg DCM. From the second day, all digesters were fed as follows: 0.7, 0.239, and 92 0.210 kg DCM for R1, R2 and R3 respectively (after first removing the same amount of 93 digestate from a port at the base of the digesters) which continued for the following 21 d 94 95 adaptation period. The digesters were fed through a tube, the outlet of which was 96 submerged under the substrate level to avoid air ingress during the feeding process. Data 97 were collected after this 21 d startup period. During the data collection period, R1 was fed 0.7 kg DCM. Effluent from this digester (0.239 kg) was used to feed R2, while R3 98 99 was fed 0.210 kg DCM. Digesters were kept at ambient temperature, and the experiment 100 was run for a period of three HRT corresponding to 75 d in total.

- 101
- 102

Inoculum and Substrate

103 Inoculum in this study was sourced from the active biogas digester at the Faculty104 of Animal and Agricultural Sciences, Diponegoro University. The digester treats DCM

and operates at ambient temperature. The digested slurry from the digester was transferred
directly to the laboratory scale digesters.

Substrate was taken from dairy cows in the lactation period and was collected 107 from the farm in the Faculty of Animal and Agricultural Sciences, Diponegoro 108 109 University. Manure was diluted with tap water in the ratio 1:1.5. Manure was collected once per week and diluted with tap water directly and kept refrigerated. pH value, volatile 110 111 solids (VS) and total ammonia nitrogen (TAN) concentration in the inoculum were 7.11, 7.33% and 265.18 mg/L respectively, while pH value, VS, TAN and volatile fatty acids 112 (VFA) (C2-C5) concentration of DCM were 6.77, 7.40%, 97.98 mg/L and 142.93 mg/L 113 respectively. 114

115

116

Analytical Methods

Biogas from the laboratory scale bio-digesters was passed up through 0.5 L 117 infusion bottles that contained 4% NaOH solution in order to absorb CO₂ using 5 ml 118 119 diameter Teflon tubing. Methane production was measured on a daily basis by collecting 120 the gas using 5 L Tedlar gas bags using a water displacement method (Figure 1). The 121 procedures to quantify gas production were: 1) valve to pump was in open position. 2) water pump was switched on. Therefore air in the measuring glass head space was 122 123 removed, and the headspace was filled up with tap water. 3) valve to pump was closed. 4) water pump was switched off. 5) valve to Tedlar gas bag was opened therefore the 124 125 methane in the Tedlar gas bag will move to the head space of the measuring glass. 6) gas 126 volume was read in the measuring glass scale. When the gas volume in the Tedlar gas bag 127 exceeded the measuring glass volume, steps 1-6 were repeated. The net gas production was corrected to STP conditions. 128

| 129 | Daily maximum and minimum ambient temperature was recorded using a digital |
|---|--|
| 130 | hygrometer thermometer HTC-2 (Taiwan). Sample pH value was measured using a pH |
| 131 | meter (Hanna® pH meter). Dry matter (DM) contents of samples were analyzed by drying |
| 132 | at 105°C for 7 h. Ash was determined by combusting the dried samples at 550°C for 6 h, |
| 133 | and VS was calculated by subtracting the ash weight from the DM (APHA,1995). TAN |
| 134 | concentration was measured using photometric kits (HACH® USA: DOC316.53.01077) |
| 135 | at 655 nm. VFA were determined using gas chromatography (Shimadzu GC-8). The |
| 136 | collected data were statistically analyzed using ANOVA with 95% confidence level. |
| 137 | Duncan's multiple range tests were used in post ANOVA analysis when differences were |
| 138 | found to be significant (Gomez and Gomez, 2007). |
| 139 | |
| 140 | RESULTS |
| | |
| 141 | Ambient Temperature Variation |
| 141 142 | Ambient Temperature Variation Average daily maximum-minimum ambient temperature throughout the |
| 141 142 143 | Ambient Temperature Variation Average daily maximum-minimum ambient temperature throughout the experiment was 36.55°C and 20.93°C, respectively (Figure 2). There was 15.63°C |
| 141 142 143 144 | Ambient Temperature Variation Average daily maximum-minimum ambient temperature throughout the experiment was 36.55°C and 20.93°C, respectively (Figure 2). There was 15.63°C temperature difference between maximum temperature in day time and minimum |
| 141 142 143 144 145 | Ambient Temperature Variation Average daily maximum-minimum ambient temperature throughout the experiment was 36.55°C and 20.93°C, respectively (Figure 2). There was 15.63°C temperature difference between maximum temperature in day time and minimum temperature in the night time and the ambient temperature in this study therefore falls into |
| 141 142 143 144 145 146 | Ambient Temperature Variation Average daily maximum-minimum ambient temperature throughout the experiment was 36.55°C and 20.93°C, respectively (Figure 2). There was 15.63°C temperature difference between maximum temperature in day time and minimum temperature in the night time and the ambient temperature in this study therefore falls into the mesophilic category (Burton and Turner, 2003). |
| 141 142 143 144 145 146 147 | Ambient Temperature Variation Average daily maximum-minimum ambient temperature throughout the experiment was 36.55°C and 20.93°C, respectively (Figure 2). There was 15.63°C temperature difference between maximum temperature in day time and minimum temperature in the night time and the ambient temperature in this study therefore falls into the mesophilic category (Burton and Turner, 2003). |
| 141 142 143 144 145 146 147 148 | Ambient Temperature Variation Average daily maximum-minimum ambient temperature throughout the experiment was 36.55°C and 20.93°C, respectively (Figure 2). There was 15.63°C temperature difference between maximum temperature in day time and minimum temperature in the night time and the ambient temperature in this study therefore falls into the mesophilic category (Burton and Turner, 2003). Methane production |
| 141 142 143 144 145 146 147 148 149 | Ambient Temperature Variation Average daily maximum-minimum ambient temperature throughout the experiment was 36.55°C and 20.93°C, respectively (Figure 2). There was 15.63°C temperature difference between maximum temperature in day time and minimum temperature in the night time and the ambient temperature in this study therefore falls into the mesophilic category (Burton and Turner, 2003). Methane production The methane production of the three bio-digesters throughout the experiment is |
| 141 142 143 144 145 146 147 148 149 150 | Ambient Temperature Variation Average daily maximum-minimum ambient temperature throughout the experiment was 36.55°C and 20.93°C, respectively (Figure 2). There was 15.63°C temperature difference between maximum temperature in day time and minimum temperature in the night time and the ambient temperature in this study therefore falls into the mesophilic category (Burton and Turner, 2003). Methane production The methane production of the three bio-digesters throughout the experiment is presented in Figure 3. The mean methane yields were 14.31 L/kg VS, 132.82 L/kg VS, |
| 141 142 143 144 145 146 147 148 149 150 151 | Ambient Temperature Variation Average daily maximum-minimum ambient temperature throughout the experiment was 36.55°C and 20.93°C, respectively (Figure 2). There was 15.63°C temperature difference between maximum temperature in day time and minimum temperature in the night time and the ambient temperature in this study therefore falls into the mesophilic category (Burton and Turner, 2003). Methane production The methane production of the three bio-digesters throughout the experiment is presented in Figure 3. The mean methane yields were 14.31 L/kg VS, 132.82 L/kg VS, and 146 L/kg VS for R1, R2 and R3 respectively. Total methane yield of R1 and R2 (R _{TS}) |

digesters with 16 d incubation period at 55°C showed that methane production of DCM was 145.03 L/kg VS while the study from Sutaryo *et al.* (2014) using continuous digesters with 20 d HRT at 35°C found that methane production of DCM was 177 L/kg VS. Both those studies were performed at constant mesophilic temperature while the study presented here was performed at ambient variable mesophilic temperatures. However the result of this study is similar to those previous results.

- 159
- 160

Parameters in the Liquid Phase

Total VFA concentration and pH value of digested slurry are presented in Table 1. The mean total VFA concentration was 160.74; 48.23; 39.19 mg/L for R1, R2, and R3, respectively. Total VFA concentration of digested slurry in R1 was significantly higher (p<0.05) than that in R2 and R3 (Table 1). TAN concentration concentrations of digested slurry in this study were 137.85; 178.96; 185.86 mg/L for R1, R2, and R3, respectively (Table 1).

Volatile solid reductions in this study were 29.85 and 28.03% for R2 and R3 respectively. Brown and Li (2013) found a VS reduction of 27% and 33% for batch of AD, treating yard waste and combination of 90% yard waste and 10% food waste respectively, and maintained at 36°C for 30 d. Meanwhile, a study from Sutaryo *et al.* (2012) found a VS reduction in range of 27-35% for a reactor treating DCM with different TS concentrations. Therefore the result of this study is in accordance with the result of the previous study.

174

DISCUSSION

175

Ambient Temperature Variation

This study was performed in July-September, and in Indonesia that period is considered to be in the dry season. A large variation temperature in AD operation in the 177 course of this study therefore has an adverse impact on the microorganism activity. Mao 178 et al. (2015) reported that the AD process is carried out by a prime balanced population 179 of various microorganisms. These microorganisms are very sensitive to environmental 180 condition changes including temperature. 181

182

183

Methane production

There was no significant effect (p>0.05) of the application of a two-phase bio-184 digester on specific methane yield in terms of kg VS of substrate added when compared 185 186 to that from the single digester configuration (Table 1). However, methane production of R_{TS} was significantly higher (p<0.05) than that in R3 in term of L/L digester volume 187 (methane production/volume active). No significant effect (p>0.05) of the application of 188 the two-stage digester than single-digester on specific methane yield in this study can be 189 190 due to anaerobic microorganisms activities in both reactors configuration operation 191 efficiently. This study used digested slurry from an active digester that operated at a 192 tropical ambient temperature, the same condition used in this study. This fact, along with the three weeks adaptation period, contributed to the efficient microorganism's activity 193 194 in both reactor configurations in this study even though there was a large temperature difference between day and night time. A study by Chae et al. (2008) found that using 195 196 batch digesters and treating swine manure, the methane production at 30 and 35°C were 197 quite similar, but it was higher by more than 13-17% than that at 25°C. Temperature 198 shocks caused a reduction in the methane production rate compared to that of the control, but it recovered rapidly. Once adapted, no significant effect on the methane production 199

was observed between the control and the temperature shock bio-digester. This fact therefore indicates that, even though methanogenic archaea are quite sensitive to temperature shock they have considerable ability to adapt to temperature changes (Chae *et al.*, 2008).

Methane production in term of digester volume of R_{TS} was 29.98% higher than 204 that in R3. The positive effect (p < 0.05) of the application of two-phase digestion on the 205 206 methane production compared to that in the single-phase reactor can be attributed to a 207 shorter HRT period in R1 and R2 than that in R3, therefore the amount of substrate added 208 to R1 and R2 was higher than that in R3. Since the amount of substrate added to R2 (0.239 kg) was higher than that in R3 (0.210 kg) and in the same time the active volume in both 209 210 digester configurations was equal (5.25 L) therefore methane production in term of digester volume R2 was higher than that in R3. In fact methane production in R_{TS} was 211 methane yield in R1 and in R2. In this present study, HRT in R1, R2 and R3 were 3 d, 22 212 d and 25 d respectively. Sinbuathong et al., (2012) reported that one of the advantages of 213 phase separation is the ability to handle a higher organic loading rate than that in a single 214 215 reactor. A similar study from Tsigkou et al. (2020) found the same phenomenon, in that 216 the application of a two-stage digester treating co-digestion of used disposable nappies and expired food product at 60:40 (v/v) ratio, working at mesophilic condition $(37\pm0.5^{\circ}C)$ 217 218 and 15 d HRT the energy production was 18.5% higher than that in the single reactor.

- 219
- 220

Parameters in the Liquid Phase

During bioconversion of organic matter in AD system there are four steps, namely hydrolysis, acidogenesis, acetogenesis and methanogenesis. In a two stage digester configuration, the first digester serves as the acidogenic phase (Sinbuatong *et al.*, 2012), therefore the VFA concentration will be higher than that in the second digester. A higher
total VFA concentration in R1 than that on other reactor in this study is in accordance
with Baldi *et al.* (2019) who found that total VFA concentration of digested slurry in a
fermentative digester was significantly higher than that of digested slurry from
methanogenic digester.

The higher VFA concentration of R1-digested slurry gave consequences on the lower pH value (p<0.05) than that in R2 and R3-digested slurry. The mean pH values of digested slurry in this recent study were 6.46; 6.84 and 6.89 for R1, R2 and R3 respectively. The pH value of R2 and R3 in this recent study was in the range of a stable AD process. Mao *et al.* (2015) reported that the ideal pH value for AD process is in the range of 6.8 to 7.4.

Ammonia is one of the essential nutrients for the growth of microorganisms, 235 however it can inhibit the AD process if it is available at high concentrations (Yenigün 236 and Demirel, 2013). Under mesophilic conditions (35°C), the TAN inhibitory threshold 237 238 was in the concentrations of around 1700-1800 mg/L for unacclimated inoculum 239 (Yenigün and Demirel, 2013). TAN concentration of digested slurry in R1 was 240 significantly lower (p<0.05) than that in R2 and R3. This fact can be attributed to a shorter HRT in R1 than that in R2 and R3 therefore microorganisms in R2 and R3 can degrade 241 242 more protein in the substrate, subsequently producing more ammonia. However TAN concentrations of digested slurry from all digester in this study were below the inhibitory 243 244 level as reported by Yenigün and Demirel (2013).

There was no significant effect (p>0.05) of the application two stage compared to single stage digesters on the VS reduction. No significant effect of phase separation on volatile solid reduction in this study suggests that microorganisms in both reactorconfigurations can work well.

- 249
- 250

CONCLUSION

251 It has been demonstrated that the application of a two-phase digester treating DCM working at a tropical ambient temperature significantly increased methane 252 production by 29.98% compared to the single stage reactor in terms of digester volume. 253 254 However, no significant effect of this digester configuration on specific methane yield in terms of VS. Both digester configurations can run properly with stable methane 255 production, low VFA, and TAN concentrations. Therefore the two-phase digester 256 257 configuration in tropical ambient temperature can be applied to increase methane production in terms of digester volume. However, to be implemented on an industrial 258 scale, further study is needed related to the addition of infrastructure to the two-phase 259 digester rather than the single reactor. 260

- 261
- 262

CONFLICT OF INTEREST

We certify that there is no conflict of interest with any financial, personal, or other relationships with other people or organization related to the material discussed in the manuscript.

- 266
- 267

ACKNOWLEDGEMENT

The authors would like to thank Diponegoro University (grant number:
109/UN7.5.5/PP/2018) for financing this study.

| 271 | REFERENCES |
|-----|--|
| 272 | Adekunle, K. F. & J. A. Okolie. 2015. A Review of Biochemical Process of Anaerobic |
| 273 | Digestion. Adv. Biosci. Biotechnol. 6:205-212. |
| 274 | APHA, 1995. Standard Methods for Examination of Water and Waste Water, 19th ed. |
| 275 | American Public Health Association, Washington, DC. |
| 276 | Bandara, W. M. K. R. T. W., T. Kindaichi, H. Satoh, M. Sasakawa, Y. Nakahara, |
| 277 | M. Takahashi, & S. Okabe. 2012. Anaerobic treatmentofmunicipal wastewater |
| 278 | at ambient temperature: Analysis of archaeal community structure and recovery |
| 279 | of dissolved methane. Water Res. 46:5756-5764. |
| 280 | Baldi, F., L. Pecorini, & R. Iannelli. 2019. Comparison of single-stage and two-stage |
| 281 | anaerobic co-digestion of food waste and activated sludge for hydrogen and |
| 282 | methane production. Renew Energy. 43:1755-1765. |
| 283 | Beneragama, N., S. A. Lateef, M. Iwasaki, T. Yamashiro, & K. Umetsu. 2013. The |
| 284 | combined effect of cefazolin and oxytertracycline on biogas production from |
| 285 | thermophilic anaerobic digestion of dairy manure. Bioresource Biotechnol. |
| 286 | 133:23-30. |
| 287 | Burton, C.H. & Turner, C., 2003. Anaerobic treatment options for animal manures. In: |
| 288 | Manure Management – Treatment Strategies for Sustainable Agriculture, 2 nd edn, |
| 289 | chapter 7. Silsoe Research Institute, as part of the EU Accompanying Measure |
| 290 | project, MATRESA, Wrest Park, Silsoe, Bedford, UK. |
| 291 | |
| 292 | Brown, D. & Y. Li. 2013. Solid state anaerobic co-digestion of yard waste and food |
| 293 | waste for biogas production. Bioresour. Technol. 127:275-280. |
| | |

| 294 | Chae, K. J., S. K. Am Jang, L. Yim, & S. Kim. 2008. The effects of digestion |
|--|---|
| 295 | temperature and temperature shock on the biogas yields from the mesophilic |
| 296 | anaerobic digestion of swine manure. Bioresour. Technol. 99:1-6. |
| 297 | Ganesh, R., M. Torrijos, P. Sousbie, A. Lugardon, J. P. Steyer, & J. P. Delg. 2014. |
| 298 | Single-phase and two-phase anaerobic digestion of fruit and vegetable waste: |
| 299 | Comparison of start-up, reactor stability and process performance. Waste Manag. |
| 300 | 34:875-885. |
| 301 | Gomez, K. A., & A. A. Gomez. 2007. Prosedur statistik untuk penelitian pertanian. |
| 302 | Translated by Sjamsuddin, E., & J. S. Baharsjah. UI Press, Jakarta. |
| 303 | Linke, B., A. Rodríguez-Abalde, C. Jost, & A. Krieg. 2015. Performance of a novel |
| 304 | two-phase continuously fed leach bed reactor for demand-based biogas |
| 305 | production from maize silage. Bioresour. Technol. 177:34-40. |
| 306 | Mao, C., Y. Feng, X. Wang, & G. Ren. 2015. Review on research achievements of |
| 307 | biogas from anaerobic digestion. Renew. Sust. Energ. Rev. 45:540-555. |
| 308 | Minale, M. & T. Worku. 2014. Anaerobic co-digestion of sanitary wastewater and |
| 309 | kitchen solid waste for biogas and fertilizer production under ambient |
| 310 | |
| | temperature: waste generated from condominium house. Int. J. Environ. Sci. |
| 311 | temperature: waste generated from condominium house. Int. J. Environ. Sci. Technol. 11(2):509-516. |
| 311 312 | temperature: waste generated from condominium house. Int. J. Environ. Sci. Technol. 11(2):509-516. Murugan, N. & P. Appavu. 2018. Investigation on low temperature biogas generation. |
| 311 312 313 | temperature: waste generated from condominium house. Int. J. Environ. Sci. Technol. 11(2):509-516. Murugan, N. & P. Appavu. 2018. Investigation on low temperature biogas generation. Int. J. ambient energy. 39:1-3. |
| 311 312 313 314 | temperature: waste generated from condominium house. Int. J. Environ. Sci. Technol. 11(2):509-516. Murugan, N. & P. Appavu. 2018. Investigation on low temperature biogas generation. Int. J. ambient energy. 39:1-3. Noorollahi, Y., M. Kheirrouz, H. F. Asl, H. Yousefi, & A. Hajinezhad. 2015. Biogas |
| 311 312 313 314 315 | temperature: waste generated from condominium house. Int. J. Environ. Sci. Technol. 11(2):509-516. Murugan, N. & P. Appavu. 2018. Investigation on low temperature biogas generation. Int. J. ambient energy. 39:1-3. Noorollahi, Y., M. Kheirrouz, H. F. Asl, H. Yousefi, & A. Hajinezhad. 2015. Biogas production potential from livestock manure in Iran. Renew. Sust. Energ. Rev. |
| 311 312 313 314 315 316 | temperature: waste generated from condominium house. Int. J. Environ. Sci. Technol. 11(2):509-516. Murugan, N. & P. Appavu. 2018. Investigation on low temperature biogas generation. Int. J. ambient energy. 39:1-3. Noorollahi, Y., M. Kheirrouz, H. F. Asl, H. Yousefi, & A. Hajinezhad. 2015. Biogas production potential from livestock manure in Iran. Renew. Sust. Energ. Rev. 50:748-754. |

| 317 | Rao, P. V., S. S. Baral, R. Dey, & S. Mutnuri. 2010. Biogas generation potential by | | | |
|-----|--|--|--|--|
| 318 | anaerobic digestion for sustainable energy development in India. Renew. Sust. | | | |
| 319 | Energ. Rev. 14:2086-2094. | | | |
| 320 | Sinbuathong, N., P. Sirirote, B. Sillapacharoenkul, J. Munakata-Marr, & S. | | | |
| 321 | Chulalaksananukul. 2012. Biogas production from two-stage anaerobic | | | |
| 322 | digestion of jatropa curcas seed cake. Energ. Source Part A. 34(22):2048-2056. | | | |
| 323 | Sutaryo, S., A. J. Ward, & H. B. Møller. 2012. Thermophilic anaerobic co-digestion of | | | |
| 324 | separated solids from acidified dairy cow manure. Bioresour. Technol. 114:195- | | | |
| 325 | 200. | | | |
| 326 | Sutaryo, S., A. J. Ward, & H. B. Møller. 2014. The effect of mixed-enzyme addition in | | | |
| 327 | anaerobic digestion on methane yield of dairy cattle manure. Environ. Technol. | | | |
| 328 | 35(19):2476-2482. | | | |
| 329 | Tsigkou, K., P. Tsafrakidou, A. Kopsahelis, D. Zagklis, C. Zafiri, & M. Kornaros. | | | |
| 330 | 2020. Used disposable nappies and expired food products valorization through | | | |
| 331 | one- & two-stage anaerobic co-digestion. Renew. Energy. 147:610-619. | | | |
| 332 | Wei, S., H. Zhang, Z. Cai, J. Xu, J. Fang, & H. Liu. 2014. Psychrophilic anaerobic co- | | | |
| 333 | digestion of highland barley straw with two animal manures at high altitude for | | | |
| 334 | enhancing biogas production. Energy convers. manag. 88:40-48. | | | |
| 335 | Yenigün, O., & B. Demirel. 2013. Ammonia inhibition in anaerobic digestion: A review. | | | |
| 336 | Process Biochem. 48:901-911. | | | |
| 337 | | | | |

338 Figure caption



Figure 1. Apparatus for measuring gas production

- 1. Tap water
- 2. Water container
- 3. Measuring glass
- 4. Measuring glass holder
- 5. Teflon tube Ø 5 mm
- 6. Valve to pump and valve to tedlar gas bag
- 7. Water pump
- 8. Switch
- 9. Tedlar gas bag



349

348

350 Figure 2. Maximum-minimum ambient temperature during experiment



Figure 3. A. Methane yield per kg VS added.



Figure 3. B. Methane yield per digester volume per day

359 **Table caption**

360 Table 1. Process parameters.

| | Methane yield | | Total VFA TAN | | VS reduction | pН |
|-----------------|----------------------------|---------------------|----------------------------|----------------------------|--------------------------|-------------------------|
| | (L/kg VS) | (L/L/d) | (mg/L) | (mg/L) | (%) | |
| R1 | 14.31±2.29 | 0.08±0.01 | 160.74 ^a ±58.95 | 137.84 ^a ±45.32 | | 6.46 ^a ±0.17 |
| R2 | 132.82±33.92 | 0.32 ± 0.07 | 48.23 ^b ±23.73 | 178.96 ^b ±23.61 | 29.85 ^a ±6.76 | $6.84^{b}\pm 0.17$ |
| R3 | 146.65 ^a ±42.47 | 0.31ª±0.08 | 39.19 ^b ±23.23 | 185.86 ^b ±23.68 | 28.03 ^a ±3.19 | 6.90 ^b ±0.28 |
| R _{TS} | 147.13 ^a ±34.29 | $0.41^{b} \pm 0.07$ | | | | |

361 a,b: Values in each column followed by the same letter are not significantly different (p>

362 0.05).

- 363 R1: First reactor of the two-phase digester
- R2: Second reactor of the two-phase bio-degester
- 365 R3: Single-phase reactor
- 366 R_{TS:} Total sum methane yield of R1 and R2

367

368

369

4. Permintaan revisi dari editor terhadap hasil perbaikan pertama



Dear Sutaryo Sutaryo, Aldila Sempana, Cristina Lestari, Alastair Ward:

It is my pleasure to inform you that your submission to Tropical Animal Science Journal, "A Performance Comparison of Single and Two Phase Biogas Digesters Treating Dairy Cattle Manure at Tropical Ambient Temperature" had been examined by Editor. Please find the comments and suggestions:

Submission URL: <u>http://journal.ipb.ac.id/index.php/tasj/authorDashboard/submission/30343</u> Username: {SauthorUsername}

If you decide to revise the manuscript, please give a response or rebuttal against each point which are suggested by Editor. The revised document should include revision note file in table form and revised manuscript in MS Word file. Please return back the documents to the editor within 14 days via OJS, we would be glad if you submit your revised manuscript as soon as possible.

If you have any questions, please contact me.

Prof. Dr. Komang G Wiryawan

FORM D



Tropical Animal Science





Faculty of Animal Science Building, IPB University (Bogor Agricultural University) JIn. Agatis, Kampus IPB Darmaga, Bogor Indonesia 16680 Phone/Fax: +62 251 8421692 E-mail: mediapeternakan@apps.ipb.ac.id; mediapeternakan@yahoo.co.id Website: http://journal.ipb.ac.id/index.php/tasj

THE REVIEW RESULT

Paper Title: Performance Comparison of Single and Two-Phase Biogas Digester Treating Dairy Cattle Manure at Tropical Ambient Temperature

Comments (please use additional paper if more space is needed)

| No | Comments | Author's response |
|----|---|-------------------|
| 1 | Authors have revised some corrections following | |
| | reviewer suggestions, but there are still some matters | |
| | that have to be revised as follow: | |
| 2 | The objective of study has to state or explain clearly in | |
| | the end of introduction | |
| 3 | Please state between results and discussions clearly | |
| | (see corrected manuscript). The Results should only | |
| | explain or elaborate the tabular data, but numbers | |
| | should not be repeated extensively within the text, | |
| | without references/discussion. | |
| | | |
| | Please see the journal's guidelines on how to write | |
| | Results and Discussions section | |
| 4 | Use variable term for research design using inference | |
| | statistic (samples) (See corrected manuscript) | |
| 5 | Please avoid statistic term in the conclusion | |
| 6 | Figure and Table have to revised following TASJ | |
| | guideline | |
| 7 | Other correction please see corrected manuscripts | |

5. Perbaikan draft publikasi atas koreksi dari editor

Surat pengantar, form revisi, dan draft revisi kedua

Dear Prof. Dr. Komang G. Wiryawan The Editor, Tropical Animal Science Journal, 7th July 2020

Subject: Resubmission of manuscript titled 'Performance Comparison of Single and Two-Phase Biogas Digester Treating Dairy Cattle Manure at Tropical Ambient Temperature' (manuscript number: TASJ_30343)

- authored by Sutaryo Sutaryo, A. N. Sempana, C. M. S. Lestari, Alastair James Ward

We herewith resubmit our paper with the title **Performance Comparison of Single and Two-Phase Biogas Digesters Treating Dairy Cattle Manure at Tropical Ambient Temperature**. The manuscript is an original article based on the experiments carried out during 2018 at Faculty Animal and Agricultural Sciences, Diponegoro University.

Thank you for the opportunity you provide us to resubmit our manuscript. The authors greatly appreciate the corrections given by the editor. In the attached new version of the manuscript (revised manuscript), changes in response to the editors' comments have been highlighted using blue text.

I thank you for your time and consideration, and look forward to hearing from you.

Thank you and best regards,

On behalf of all the authors,

Sutaryo Sutaryo Dept. of Animal Science Faculty Animal and Agricultural Sciences Diponegoro University Kampus Tembalang 50275 Email: <u>soeta@lecturer.undip.ac.id</u>

FORM D



Tropical Animal Science





Faculty of Animal Science Building, IPB University (Bogor Agricultural University) Jln. Agatis, Kampus IPB Darmaga, Bogor Indonesia 16680 Phone/Fax: +62 251 8421692 E-mail: mediapeternakan@apps.ipb.ac.id; mediapeternakan@yahoo.co.id Website: http://journal.ipb.ac.id/index.php/tasj

Paper Title: Performance Comparison of Single and Two-Phase Biogas Digester Treating Dairy Cattle Manure at Tropical Ambient Temperature

Comments (please use additional paper if more space is needed)

| No | Comments | Author's response |
|----|--|---|
| 1 | Authors have revised some corrections following reviewer suggestions, but there are still some matters that have to be revised as follow: | The authors tanks for the valuable corrections given by editor. The manuscript has been revised carefully. |
| 2 | in the end of introduction | The objective has been revised according editor suggestion Therefore the aim of this current study was to evaluate the process performance of single and two- phase biodigester treating DCM and working in this specific area. |
| 3 | Please state between results and discussions clearly (see corrected manuscript). The Results should only explain or elaborate the tabular data, but numbers should not be repeated extensively within the text, without references/discussion. Please see the journal's guidelines on how to write Results and Discussions section | The result section has been revised, no reference in the result section anymore. |
| 4 | Use variable term for research design using inference statistic (samples) (See corrected manuscript) | Thank you very much for the correction Parameters have been revised to be variables |
| 5 | Please avoid statistic term in the conclusion | The statistic term in the conclusion section has been revised to be However, there was no positive effect of this digester configuration on specific methane yield in terms of VS |
| 6 | Figure and Table have to revised following TASJ guideline | Figure and Table have been revised according editor suggestion |

| 7 | Other correction please see corrected manuscripts | Thank you for the corrections. |
|---|---|------------------------------------|
| | | Why there is no superscripcts in |
| | | the methane yield of R1 and |
| | | R2? |
| | | This experiment did not compare |
| | | methane production in R1, R2, |
| | | and R3 because direct |
| | | comparison of R1, R2 and R3 is |
| | | not possible due to the difference |
| | | in retention time |
| | | |

Performance Comparison of Single and Two-Phase Biogas Digester Treating Dairy Cattle Manure at Tropical Ambient Temperature 3

4

5

ABSTRACT

6 The biodegradation process of organic waste in anaerobic digestion can be in single or two-phase bio-reactor. This study examined the effect of different biogas 7 digester configurations (single and two-phase) on methane production of dairy cattle 8 manure (DCM) at tropical ambient temperature. Three identical reactors were used in this 9 study (R1, R2, and R3). The two-phase digesters consisted of reactors R1 and R2. R1 had 10 a 2.1 L working volume and 3 d hydraulic retention time (HRT), while R2 had 5.25 L 11 working volume and 22 d HRT (R1 and R2 had a 25 d HRT). The digested slurry of R1 12 was used to feed R2. R3 served as the single-phase digester and had 5.25 L working 13 14 volume and 25 d HRT. Methane production were 14.31, 132.82, and 146 L/kg VS for R1, R2 and R3 respectively. The results showed that there was no positive effect (p>0.05) 15 with the application of a two-phase digester configuration on specific methane yield of 16 DCM per kg volatile solids added than that in the single-reactor. Methane production was 17 detected in the first reactor of the two-phase digester configuration and the total sum 18 19 methane production of the two-phase digester was found to be 29.98% higher (p < 0.05) than that of the single reactor in terms of digester volume (0.41 VS 0.31 L/L/d). Both 20 digester configurations performed well, indicated by stable methane production, low 21 22 volatile fatty acids, and total ammonia concentrations. The two-phase bio-digester configuration can increase significantly methane production in terms of digester volume. 23 Keywords: biogas, manure, tropical ambient temperature, two-phase digester biogas. 24

- 25
- 26

INTRODUCTION

The dairy cattle industry produces large amounts of waste in the form of manure that can cause environmental pollution if not managed properly. Daily dairy cattle manure (DCM) (wet feces plus urine) excretion is 2226.5 kg/year per 610 kg of body weight (Noorollahi *et al.*, 2015). Generally, animal waste management can take place in aerobic conditions through a composting process or by anaerobic digestion (AD) to produce biogas.

Manure management through the AD process results in numerous advantages, 33 34 including the generation of renewable energy in the form of biogas. Biogas is the most efficient and effective among the various alternative sources of energy currently 35 available, it needs less capital investment per unit production cost compared to other 36 37 renewable energy sources, and it is available as a domestic resource in the rural areas. Therefore it is not subject to world price fluctuations (Rao et al., 2010). In addition, biogas 38 production from animal manure can create new enterprises and increases the income in a 39 rural area since it requires labor for production, collection and transport of AD substrates, 40 manufacture of technical equipment and the construction, operation and maintenance of 41 42 biogas plants (Adekunle and Okolie, 2015).

Technically, the AD process can take places in three different temperature ranges: 43 (1) psychrophilic (cryophilic) temperature from 10 to 20°C; (2) mesophilic temperature 44 45 from 20 to 40°C; and (3) thermophilic temperature from 40 to 60°C (Burton and Turner, 2003). Based on those temperature range criteria, the AD process can be implemented at 46 tropical ambient temperatures. Moreover, operation of AD at tropical ambient 47 temperatures offers advantages compared to the operation of AD under mesophilic or 48 thermophilic temperatures since AD operation at higher temperatures requires significant 49 energy to maintain bioreactor temperature (Bandara et al., 2012). 50
51 Among other biogas digester designs, the continuously stirred tank reactor (CSTR) design is the most commonly applied bioreactor for treating agricultural waste 52 (Linke et al., 2015). While in operation, the process of biodegradation of organic waste 53 can be in single or two-phases. The two-phase AD process has several advantages 54 compared to a single phase. These include the selection and enrichment of different 55 bacteria in each digester, increasing the stability of the process by controlling the 56 acidification stage therefore reducing the risk of overloading and the buildup of toxic 57 58 material. The first stage in the two-phase configuration can act as metabolic buffer preventing pH shock to the methanogenic microorganisms and low pH in the first stage 59 due to a high organic loading rate favors the establishment of the acidogenic phase 60 (Sinbuathong et al., 2012). On the other hand, single-phase bio-digester has also 61 advantageous as it is a simple and straightforward operation and for easier degradable 62 substrate such as fruit and vegetables waste single-phase process could be the preferred 63 rather than two-phase reactor (Ganesh et al., 2014). Although previous studies have 64 evaluated the AD process at ambient temperature (Minale and Worku, 2014; Wei et al., 65 2014; Murrugan and Appavu, 2018) and two-phase AD (Baldi et al., 2019; Tsigkou et 66 al., 2020), to the best of our knowledge there has been a lack of information regarding 67 direct comparison of single and two-phase AD of DCM at tropical ambient temperature. 68 69 Therefore the aim of this current study was to evaluate the process performance of single and two-phase biodigester treating DCM and working in this specific area. 70

- 71
- 72

MATERIALS AND METHODS

Experimental Set-Up 74 Evaluation of single and two-phase processes was conducted using three identical 75 digesters, namely R1, R2, R3. The reactors were made from stainless steel, and in order 76 to minimize temperature fluctuations between day and night time, all digesters were made 77 with double layers. The two-phase digesters consisted of reactors R1 and R2. Reactor 1 78 had a 2.1 L working volume (the minimum volume that can be applied in the reactor) and 79 80 3 d hydraulic retention (HRT), while R2 had 5.25 L working volume and 22 d HRT. Therefore in total, R1 and R2 had a 25 d HRT. R3 served as the single-phase bioreactor 81 and had 5.25 L working volume and 25 d HRT. Mao et al. (2015) reported that under 82 mesophilic conditions, an average HRT in the range of 15-30 d is required to treat waste. 83 The experiment was started by filling R1 with 1.4 kg inoculum and 0.7 kg DCM, 84 R2 with 5.011 kg inoculum, and 0.239 kg DCM and R3 with 5.040 kg inoculum and 85 0.210 kg DCM. From the second day, all digesters were fed as follows: 0.7, 0.239, and 86 0.210 kg DCM for R1, R2 and R3 respectively (after first removing the same amount of 87 digestate from a port at the base of the digesters) which continued for the following 21 d 88 adaptation period. The digesters were fed through a tube, the outlet of which was 89 submerged under the substrate level to avoid air ingress during the feeding process. Data 90 91 were collected after this 21 d startup period. During the data collection period, R1 was fed 0.7 kg DCM. Effluent from this digester (0.239 kg) was used to feed R2, while R3 92 was fed 0.210 kg DCM. Digesters were kept at ambient temperature, and the experiment 93 94 was run for a period of three HRT corresponding to 75 d in total.

- 95
- 96

Inoculum and Substrate

97 Inoculum in this study was sourced from the active biogas digester at the Faculty
98 of Animal and Agricultural Sciences, Diponegoro University. The digester treats DCM
99 and operates at ambient temperature. The digested slurry from the digester was transferred
100 directly to the laboratory scale digesters.

Substrate was taken from dairy cows in the lactation period and was collected 101 from the farm in the Faculty of Animal and Agricultural Sciences, Diponegoro 102 University. Manure was diluted with tap water in the ratio 1:1.5. Manure was collected 103 104 once per week and diluted with tap water directly and kept refrigerated. pH value, volatile 105 solids (VS) and total ammonia nitrogen (TAN) concentration in the inoculum were 7.11, 7.33% and 265.18 mg/L respectively, while pH value, VS, TAN and volatile fatty acids 106 107 (VFA) (C2-C5) concentration of DCM were 6.77, 7.40%, 97.98 mg/L and 142.93 mg/L respectively. 108

109

110

Analytical Methods

Biogas from the laboratory scale bio-digesters was passed up through 0.5 L 111 112 infusion bottles that contained 4% NaOH solution in order to absorb CO₂ using 5 ml diameter Teflon tubing. Methane production was measured on a daily basis by collecting 113 the gas using 5 L Tedlar gas bags using a water displacement method (Figure 1). The 114 115 procedures to quantify gas production were: 1) valve to pump was in open position. 2) water pump was switched on. Therefore air in the measuring glass head space was 116 removed, and the headspace was filled up with tap water. 3) valve to pump was closed. 117 118 4) water pump was switched off. 5) valve to Tedlar gas bag was opened therefore the methane in the Tedlar gas bag will move to the head space of the measuring glass. 6) gas 119 volume was read in the measuring glass scale. When the gas volume in the Tedlar gas bag 120

exceeded the measuring glass volume, steps 1-6 were repeated. The net gas productionwas corrected to STP conditions.

| 123 | Daily maximum and minimum ambient temperature was recorded using a digital |
|-----|--|
| 124 | hygrometer thermometer HTC-2 (Taiwan). Sample pH value was measured using a pH |
| 125 | meter (Hanna® pH meter). Dry matter (DM) contents of samples were analyzed by drying |
| 126 | at 105°C for 7 h. Ash was determined by combusting the dried samples at 550°C for 6 h, |
| 127 | and VS was calculated by subtracting the ash weight from the DM (APHA,1995). TAN |
| 128 | concentration was measured using photometric kits (HACH® USA: DOC316.53.01077) |
| 129 | at 655 nm. VFA were determined using gas chromatography (Shimadzu GC-8). The |
| 130 | collected data were statistically analyzed using ANOVA with 95% confidence level. |
| 131 | Duncan's multiple range tests were used in post ANOVA analysis when differences were |
| 132 | found to be significant (Gomez and Gomez, 2007). |
| 133 | |
| 134 | RESULTS |
| 135 | Ambient Temperature Variation |

Average daily maximum-minimum ambient temperature throughout the experiment was 36.55°C and 20.93°C, respectively (Figure 2). There was 15.63°C temperature difference between maximum temperature in day time and minimum temperature in the night in this study.

- 140
- 141
 Methane production
- The methane production of the three bio-digesters throughout the experiment ispresented in Figure 3. The mean methane yields were 14.31 L/kg VS, 132.82 L/kg VS,

| 144 | and 146 L/kg VS for R1, R2 and R3 respectively. Total methane yield of R1 and R2 (R_{TS}) |
|-----|---|
| 145 | was 147.13 L/kg VS (Table 1). |

| 147 | Variables in the Liquid Phase |
|-----|--|
| 148 | Total VFA concentration and pH value of digested slurry are presented in Table |
| 149 | 1. The mean total VFA concentration was 160.74; 48.23; 39.19 mg/L for R1, R2, and R3, |
| 150 | respectively. Total VFA concentration of digested slurry in R1 was significantly higher |
| 151 | (p<0.05) than that in R2 and R3 (Table 1). TAN concentration concentrations of digested |
| 152 | slurry in this study were 137.85; 178.96; 185.86 mg/L for R1, R2, and R3, respectively |
| 153 | (Table 1). Volatile solid reductions in this study were 29.85 and 28.03% for R2 and R3 |
| 154 | respectively. |
| 155 | |
| 156 | DISCUSSION |
| 157 | Ambient Temperature Variation |
| 158 | This study was performed in July-September, and in Indonesia that period is |
| 159 | considered to be in the dry season. A large variation temperature in AD operation in the |
| 160 | course of this study therefore has an adverse impact on the microorganism activity. Mao |
| 161 | et al. (2015) reported that the AD process is carried out by a prime balanced population |
| 162 | of various microorganisms. These microorganisms are very sensitive to environmental |
| 163 | condition changes including temperature. The ambient temperature in this study (Figure |
| 164 | 2) therefore falls into the mesophilic category (Burton and Turner, 2003). |
| 165 | |
| 166 | Methane production |

167 There was no significant effect of the application of a two-phase bio-digester on specific methane yield in terms of kg VS of substrate added when compared to that from 168 the single digester configuration (Table 1). However, methane production of R_{TS} was 169 significantly higher (p<0.05) than that in R3 in term of L/L digester volume (methane 170 production/volume active). No significant effect of the application of the two-stage 171 digester than single-digester on specific methane yield in this study can be due to 172 anaerobic microorganisms activities in both reactors configuration operation efficiently. 173 174 This study used digested slurry from an active digester that operated at a tropical ambient temperature, the same condition used in this study. This fact, along with the three weeks 175 adaptation period, contributed to the efficient microorganism's activity in both reactor 176 177 configurations in this study even though there was a large temperature difference between day and night time. A study by Chae et al. (2008) found that using batch digesters and 178 treating swine manure, the methane production at 30 and 35°C were quite similar, but it 179 was higher by more than 13%-17% than that at 25°C. Temperature shocks caused a 180 reduction in the methane production rate compared to that of the control, but it recovered 181 182 rapidly. Once adapted, no significant effect on the methane production was observed between the control and the temperature shock bio-digester. This fact therefore indicates 183 that, even though methanogenic archaea are quite sensitive to temperature shock they 184 185 have considerable ability to adapt to temperature changes (Chae et al., 2008).

A study from Beneragama *et al.* (2013) using batch digesters with 16 d incubation period at 55°C showed that methane production of DCM was 145.03 L/kg VS while the study from Sutaryo *et al.* (2014) using continuous digesters with 20 d HRT at 35°C found that methane production of DCM was 177 L/kg VS. Both those studies were performed at constant mesophilic temperature while the study presented here was performed at

ambient variable mesophilic temperatures. However the result of this study is similar tothose previous results.

Methane production in term of digester volume of R_{TS} was 29.98% higher than 193 that in R3. The positive effect (p < 0.05) of the application of two-phase digestion on the 194 methane production compared to that in the single-phase reactor can be attributed to a 195 shorter HRT period in R1 and R2 than that in R3, therefore the amount of substrate added 196 to R1 and R2 was higher than that in R3. Since the amount of substrate added to R2 (0.239 197 198 kg) was higher than that in R3 (0.210 kg) and in the same time the active volume in both digester configurations was equal (5.25 L) therefore methane production in term of 199 digester volume R2 was higher than that in R3. In fact methane production in R_{TS} was 200 201 methane yield in R1 and in R2. In this present study, HRT in R1, R2 and R3 were 3 d, 22 d and 25 d respectively. Sinbuathong et al., (2012) reported that one of the advantages of 202 phase separation is the ability to handle a higher organic loading rate than that in a single 203 reactor. A similar study from Tsigkou et al. (2020) found the same phenomenon, in that 204 the application of a two-stage digester treating co-digestion of used disposable nappies 205 206 and expired food product at 60:40 (v/v) ratio, working at mesophilic condition $(37\pm0.5^{\circ}C)$ and 15 d HRT the energy production was 18.5% higher than that in the single reactor. 207

208

Variables in the Liquid Phase

During bioconversion of organic matter in AD system there are four steps, namely hydrolysis, acidogenesis, acetogenesis and methanogenesis. In a two stage digester configuration, the first digester serves as the acidogenic phase (Sinbuatong *et al.*, 2012), therefore the VFA concentration will be higher than that in the second digester. A higher total VFA concentration in R1 than that on other reactor in this study is in accordance with Baldi *et al.* (2019) who found that total VFA concentration of digested slurry in a 215 fermentative digester was significantly higher than that of digested slurry from 216 methanogenic digester.

The higher VFA concentration of R1-digested slurry gave consequences on the lower pH value (p<0.05) than that in R2 and R3-digested slurry. The mean pH values of digested slurry in this recent study were 6.46; 6.84 and 6.89 for R1, R2 and R3 respectively. The pH value of R2 and R3 in this recent study was in the range of a stable AD process. Mao *et al.* (2015) reported that the ideal pH value for AD process is in the range of 6.8 to 7.4.

223 Ammonia is one of the essential nutrients for the growth of microorganisms, however it can inhibit the AD process if it is available at high concentrations (Yenigün 224 225 and Demirel, 2013). Under mesophilic conditions (35°C), the TAN inhibitory threshold was in the concentrations of around 1700-1800 mg/L for unacclimated inoculum 226 (Yenigün and Demirel, 2013). TAN concentration of digested slurry in R1 was 227 significantly lower (p<0.05) than that in R2 and R3. This fact can be attributed to a shorter 228 HRT in R1 than that in R2 and R3 therefore microorganisms in R2 and R3 can degrade 229 230 more protein in the substrate, subsequently producing more ammonia. However TAN concentrations of digested slurry from all digester in this study were below the inhibitory 231 232 level as reported by Yenigün and Demirel (2013).

There was no significant effect of the application two stage compared to single stage digesters on the VS reduction. No significant effect of phase separation on volatile solid reduction in this study suggests that microorganisms in both reactor configurations can work well. Brown and Li (2013) found a VS reduction of 27% and 33% for batch of AD, treating yard waste and combination of 90% yard waste and 10% food waste respectively, and maintained at 36°C for 30 d. Meanwhile, a study from Sutaryo *et al.*

| 239 | (2012) found a VS reduction in range of 27-35% for a reactor treating DCM with different |
|-----|---|
| 240 | TS concentrations. Therefore the result of this study is in accordance with the result of |
| 241 | the previous study. |

- 242
- 243

CONCLUSION

It has been demonstrated that the application of a two-phase digester treating 244 DCM working at a tropical ambient temperature significantly increased methane 245 246 production by 29.98% compared to the single stage reactor in terms of digester volume. However, there was no positive effect of this digester configuration on specific methane 247 yield in terms of VS. Both digester configurations can run properly with stable methane 248 249 production, low VFA, and TAN concentrations. Therefore the two-phase digester configuration in tropical ambient temperature can be applied to increase methane 250 production in terms of digester volume. However, to be implemented on an industrial 251 scale, further study is needed related to the addition of infrastructure to the two-phase 252 digester rather than the single reactor. 253

- 254
- 255

CONFLICT OF INTEREST

We certify that there is no conflict of interest with any financial, personal, or other relationships with other people or organization related to the material discussed in the manuscript.

259

260

ACKNOWLEDGEMENT

The authors would like to thank Diponegoro University (grant number:
109/UN7.5.5/PP/2018) for financing this study.

| 263 | |
|-----|--|
| 264 | REFERENCES |
| 265 | Adekunle, K. F. & J. A. Okolie. 2015. A Review of Biochemical Process of Anaerobic |
| 266 | Digestion. Adv. Biosci. Biotechnol. 6:205-212. |
| 267 | APHA, 1995. Standard Methods for Examination of Water and Waste Water, 19th ed. |
| 268 | American Public Health Association, Washington, DC. |
| 269 | Bandara, W. M. K. R. T. W., T. Kindaichi, H. Satoh, M. Sasakawa, Y. Nakahara, |
| 270 | M. Takahashi, & S. Okabe. 2012. Anaerobic treatmentofmunicipal wastewater |
| 271 | at ambient temperature: Analysis of archaeal community structure and recovery |
| 272 | of dissolved methane. Water Res. 46:5756-5764. |
| 273 | Baldi, F., L. Pecorini, & R. Iannelli. 2019. Comparison of single-stage and two-stage |
| 274 | anaerobic co-digestion of food waste and activated sludge for hydrogen and |
| 275 | methane production. Renew Energy. 43:1755-1765. |
| 276 | Beneragama, N., S. A. Lateef, M. Iwasaki, T. Yamashiro, & K. Umetsu. 2013. The |
| 277 | combined effect of cefazolin and oxytertracycline on biogas production from |
| 278 | thermophilic anaerobic digestion of dairy manure. Bioresource Biotechnol. |
| 279 | 133:23-30. |
| 280 | Burton, C.H. & Turner, C., 2003. Anaerobic treatment options for animal manures. In: |
| 281 | Manure Management – Treatment Strategies for Sustainable Agriculture, 2 nd edn, |
| 282 | chapter 7. Silsoe Research Institute, as part of the EU Accompanying Measure |
| 283 | project, MATRESA, Wrest Park, Silsoe, Bedford, UK. |
| 284 | Brown, D. & Y. Li. 2013. Solid state anaerobic co-digestion of yard waste and food |
| | |

285 waste for biogas production. Bioresour. Technol. 127:275-280.

| 286 | Chae, K. J., S. K. Am Jang, L. Yim, & S. Kim. 2008. The effects of digestion |
|-----|---|
| 287 | temperature and temperature shock on the biogas yields from the mesophilic |
| 288 | anaerobic digestion of swine manure. Bioresour. Technol. 99:1-6. |
| 289 | Ganesh, R., M. Torrijos, P. Sousbie, A. Lugardon, J. P. Steyer, & J. P. Delg. 2014. |
| 290 | Single-phase and two-phase anaerobic digestion of fruit and vegetable waste: |
| 291 | Comparison of start-up, reactor stability and process performance. Waste Manag. |
| 292 | 34:875-885. |
| 293 | Gomez, K. A., & A. A. Gomez. 2007. Prosedur statistik untuk penelitian pertanian. |
| 294 | Translated by Sjamsuddin, E., & J. S. Baharsjah. UI Press, Jakarta. |
| 295 | Linke, B., A. Rodríguez-Abalde, C. Jost, & A. Krieg. 2015. Performance of a novel |
| 296 | two-phase continuously fed leach bed reactor for demand-based biogas |
| 297 | production from maize silage. Bioresour. Technol. 177:34-40. |
| 298 | Mao, C., Y. Feng, X. Wang, & G. Ren. 2015. Review on research achievements of |
| 299 | biogas from anaerobic digestion. Renew. Sust. Energ. Rev. 45:540-555. |
| 300 | Minale, M. & T. Worku. 2014. Anaerobic co-digestion of sanitary wastewater and |
| 301 | kitchen solid waste for biogas and fertilizer production under ambient |
| 302 | temperature: waste generated from condominium house. Int. J. Environ. Sci. |
| 303 | Technol. 11(2):509-516. |
| 304 | Murugan, N. & P. Appavu. 2018. Investigation on low temperature biogas generation. |
| 305 | Int. J. ambient energy. 39:1-3. |
| 306 | Noorollahi, Y., M. Kheirrouz, H. F. Asl, H. Yousefi, & A. Hajinezhad. 2015. Biogas |
| 307 | production potential from livestock manure in Iran. Renew. Sust. Energ. Rev. |
| 308 | 50:748-754. |
| | |

| 309 | Rao, P. V., S. S. Baral, R. Dey, & S. Mutnuri. 2010. Biogas generation potential by |
|-----|--|
| 310 | anaerobic digestion for sustainable energy development in India. Renew. Sust. |
| 311 | Energ. Rev. 14:2086-2094. |
| 312 | Sinbuathong, N., P. Sirirote, B. Sillapacharoenkul, J. Munakata-Marr, & S. |
| 313 | Chulalaksananukul. 2012. Biogas production from two-stage anaerobic |
| 314 | digestion of jatropa curcas seed cake. Energ. Source Part A. 34(22):2048-2056. |
| 315 | Sutaryo, S., A. J. Ward, & H. B. Møller. 2012. Thermophilic anaerobic co-digestion of |
| 316 | separated solids from acidified dairy cow manure. Bioresour. Technol. 114:195- |
| 317 | 200. |
| 318 | Sutaryo, S., A. J. Ward, & H. B. Møller. 2014. The effect of mixed-enzyme addition in |
| 319 | anaerobic digestion on methane yield of dairy cattle manure. Environ. Technol. |
| 320 | 35(19):2476-2482. |
| 321 | Tsigkou, K., P. Tsafrakidou, A. Kopsahelis, D. Zagklis, C. Zafiri, & M. Kornaros. |
| 322 | 2020. Used disposable nappies and expired food products valorization through |
| 323 | one- & two-stage anaerobic co-digestion. Renew. Energy. 147:610-619. |
| 324 | Wei, S., H. Zhang, Z. Cai, J. Xu, J. Fang, & H. Liu. 2014. Psychrophilic anaerobic co- |
| 325 | digestion of highland barley straw with two animal manures at high altitude for |
| 326 | enhancing biogas production. Energy convers. manag. 88:40-48. |
| 327 | Yenigün, O., & B. Demirel. 2013. Ammonia inhibition in anaerobic digestion: A review. |
| 328 | Process Biochem. 48:901-911. |
| 329 | |
| 330 | 1 Tap water |
| 33 | 2. Water container |
| 33: | 3. Measuring glass |
| | a 4 holder |
| | 5. Teflon tube Ø 5 mm |
| | 6. Valve to pump and |
| | valve to tedlar gas bag |
| | 5 6 7 7. Water pump |
| | 8. Switch |
| | 0 Tadler and has |

TASJ-30343_Revised by Author







340 Figure 2. Maximum-minimum ambient temperature during experiment. ■: maximum,

▲ : minimum.





Figure 3. A. Methane yield per kg VS added. B. Methane yield per digester volume per
day. ▲: R1, ♦: R2, ×: R3, *:R_{TS}.

351 Table 1. Methan yield, Total VFA, TAN, VS reduction and pH of some reactors Reactors Variables

| | | Methane | yield | Total VFA | TAN | VS reduction | pН |
|-----------------|--------------------|--------------------------------|-----------------------|----------------------------|--------------------------------|--------------------------|------------------------|
| | | (L/kg VS) | (L/L/d) | (mg/L) | (mg/L) | (%) | |
| R1 | | 14.31±2.29 | 0.08±0.01 | 160.74 ^a ±58.95 | 137.84 ^a ±45.32 | | 6.46±0.17 ^a |
| R2 | | 132.82±33.92 | 0.32±0.07 | 48.23 ^b ±23.73 | 178.96 ^b ±23.61 | 29.85 ^a ±6.76 | $6.84{\pm}0.17^{b}$ |
| R3 | | 146.65±42.47 | $0.31{\pm}0.08^{a}$ | 39.19 ^b ±23.23 | 185.86 ^b ±23.68 | 28.03 ^a ±3.19 | $6.90{\pm}0.28^{b}$ |
| R _{TS} | | 147.13±34.29 | $0.41 {\pm} 0.07^{b}$ | | | | |
| 352 | Note: ^a | ^{a,b} : Values in the | same column fo | ollowed by the dif | ferent superscript | are significantly | |
| 353 | | different (p< 0. | 05). VFA: Vol | atile fatty acid, T | AN: Total ammon | ia nitrogen, VS: | |
| 354 | | Volatile solid, | R1: First reacto | or of the two-phas | se digester, R2: Se | econd reactor of | |
| 355 | | the two-phase | bio-degester, H | R3: Single-phase | reactor, R _{TS:} Tota | al sum methane | |
| 356 | | yield of R1 and | R2. | | | | |
| 357 | | | | | | | |
| 358 | | | | | | | |
| 359 | | | | | | | |
| 360 | | | | | | | |
| | | | | | | | |

6. Draft publikasi dinyatakan diterima untuk dipublikasikan



7. Permintaan copyediting dari editor



8. Pengiriman draft hasil copyediting dari penulis

5 To: Prof. Dr. Ir. Komang G. Wiryawan <kgwinyawan@yahoo.com>

Fri 10/30/2020 12:38 PM

.

1.0

Dear Prof. Dr. Komang G. Wiryawan The Editor, Tropical Animal Science Journal,

Subject: Resubmission of manuscript titled 'Performance Comparison of Single and Two-Phase Biogas Digester Treating Dairy Cattle Manure at Tropical Ambient Temperature' (manuscript number: TASI_30343) - authored by Sutaryo Sutaryo, A. N. Sempana, C. M. S. Lestari, Alastair James Ward

We herewith resubmit our paper with the title Performance Comparison of Single and Two-Phase Biogas Digesters Treating Dairy Cattle Manure at Tropical Ambient Temperature. The manuscript is an original article based on the experiments carried out during 2018 at Faculty Animal and Agricultural Sciences, Diponegoro University.

Thank you for the opportunity you provide us to resubmit our manuscript. The authors greatly appreciate the corrections given by the editor.

L22, P:1 : (p>0.05) has been deleted, method for ANOVA has been added in L142, P:7, Gomez and Gomez has been changed to be Gomez & Gomez (L144, P:7), L:266-268, P:12 has been deleted, L:380, P:20 row has been changed to be column.

I thank you for your time and consideration, and look forward to hearing from you.

Thank you and best regards,

On behalf of all the authors,

Sutarvo Sutarvo

| 1 2 2 | Performance Comparison of Single and Two-Phase Biogas Digesters Treating Dairy Cattle Manure at Tropical Ambient Temperature |
|-------------|---|
| 3 4 5 | S. Sutaryo ^{a,*} , A. N. Sempana ^a , C. M. S. Lestari ^a , A. J. Ward ^b |
| 6 | ^a Department of Animal Science, Faculty of Animal and Agricultural Sciences, |
| 7 | Diponegoro University, Semarang, Indonesia |
| 8 | ^b Department of Engineering, Faculty of Science and Technology, Aarhus University, |
| 9 | Aarhus, Denmark |
| 10 | *Corresponding author: soeta@lecturer.undip.ac.id; sutaryoundip@yahoo.com |
| 11 | ABSTRACT |
| 12 | The biodegradation process of organic waste in anaerobic digestion can be in a |
| 13 | single or two-phase bio-reactor. This study examined the effect of different biogas |
| 14 | digester configurations (single and two-phase) on methane production of dairy cattle |
| 15 | manure (DCM) at tropical ambient temperature. Three identical reactors were used in |
| 16 | this study (R1, R2, and R3). The two-phase digesters consisted of reactors R1 and R2. |
| 17 | R1 had a 2.1 L working volume and 3 d hydraulic retention time (HRT), while R2 had |
| 18 | 5.25 L working volume and 22 d HRT (R1 and R2 had a 25 d HRT). The digested |
| 19 | slurry of R1 was used to feed R2. R3 served as the single-phase digester and had 5.25 L |
| 20 | working volume and 25 d HRT. Methane production were 14.31, 132.82, and 146 L/kg |
| 21 | VS for R1, R2, and R3, respectively. The results showed that there was no positive |
| 22 | effect of the application of a two-phase digester configuration on the specific methane |
| 23 | yield of DCM per kg volatile solids added than that in the single-reactor. Methane |
| 24 | production was detected in the first reactor of the two-phase digester configuration and |
| 25 | the total methane production of the two-phase digester was found to be 29.98% higher |
| 26 | (p<0.05) than that of the single reactor in terms of digester volume (0.41 VS 0.31 |
| 27 | L/L/d). Both digester configurations performed well, indicated by a stable methane |

production and low volatile fatty acids and total ammonia concentrations. The twophase bio-digester configuration can significantly increase methane production in terms
of digester volume.

31 **Keywords:** biogas; manure; tropical ambient temperature; two-phase digester biogas

- 32
- 33

INTRODUCTION

The dairy cattle industry produces large amounts of waste in the form of manure that can cause environmental pollution if it is not managed properly. Daily dairy cattle manure (DCM) (wet feces plus urine) excretion is 2226.5 kg/year per 610 kg of body weight (Noorollahi *et al.*, 2015). Generally, animal waste management can take place in aerobic conditions through a composting process or by anaerobic digestion (AD) to produce biogas.

Manure management through the AD process results in numerous advantages, 40 including the generation of renewable energy in the form of biogas. Biogas is the most 41 efficient and effective among the various alternative sources of energy currently 42 43 available, it needs less capital investment per unit production cost compared to the other renewable energy sources, and it is available as a domestic resource in the rural areas. 44 Therefore, it is not subject to world price fluctuations (Rao et al., 2010). In addition, 45 46 biogas production from animal manure can create new enterprises and increases the income in a rural area since it requires labor for production, collection and transport of 47 AD substrates, manufacture of technical equipment and the construction, operation, and 48 49 maintenance of biogas plants (Adekunle & Okolie, 2015).

50 Technically, the AD process can take place in three different temperature ranges:
51 (1) psychrophilic (cryophilic) temperature from 10°C to 20°C; (2) mesophilic

temperature from 20°C to 40°C; and (3) thermophilic temperature from 40°C to 60°C (Burton & Turner, 2003). Based on those temperature-range criteria, the AD process can be implemented at tropical ambient temperatures. Moreover, the operation of AD at tropical ambient temperatures offers advantages compared to the operation of AD under mesophilic or thermophilic temperatures since AD operation at higher temperatures requires a significant amount of energy to maintain bioreactor temperature (Bandara *et al.*, 2012).

Among the other biogas-digester designs, the continuously stirred-tank reactor 59 (CSTR) design is the most commonly applied bioreactor for treating agricultural waste 60 (Linke et al., 2015). While in operation, the process of biodegradation of organic waste 61 can be in single or two-phases. The two-phase AD process has several advantages 62 compared to a single phase. These include the selection and enrichment of different 63 bacteria in each digester, increasing the stability of the process by controlling the 64 acidification stage, therefore reducing the risk of overloading and the build up of toxic 65 material. The first stage in the two-phase configuration can act as a metabolic buffer 66 67 preventing pH shock to the methanogenic microorganisms and low pH in the first stage since a high organic loading rate favors the establishment of the acidogenic phase 68 (Sinbuathong et al., 2012). On the other hand, single-phase biodigester has also 69 70 advantageous as it is a simple and straightforward operation and for an easier degradable substrate such as fruit and vegetable waste, single-phase process could be 71 the preferred choice rather than two-phase reactor (Ganesh et al., 2014). Although 72 73 previous studies have evaluated the AD process at ambient temperature (Minale & Worku, 2014; Wei et al., 2014; Murrugan and Appavu, 2018) and two-phase AD (Baldi 74 et al., 2019; Tsigkou et al., 2020), to the best of our knowledge there has been a lack of 75

information regarding to a direct comparison of single and two-phase AD of DCM in
tropical ambient temperature. Therefore, the aim of this current study was to evaluate
the process performance of single and two-phase biodigesters treating DCM and
working in this specific area.

80

MATERIALS AND METHODS

83

Experimental Set-Up

Evaluation of single and two-phase processes was conducted using three 84 identical digesters, namely R1, R2, and R3. The reactors were made from stainless steel, 85 and in order to minimize temperature fluctuations between day and night times, all 86 digesters were made with double layers. The two-phase digesters consisted of reactors 87 R1 and R2. Reactor 1 had a 2.1 L working volume (the minimum volume that can be 88 89 applied in the reactor) and 3 d hydraulic retention (HRT), while R2 had 5.25 L working volume and 22 d HRT. Therefore in total, R1 and R2 had a 25 d HRT. R3 served as the 90 single-phase bioreactor and had 5.25 L working volume and 25 d HRT. Mao et al. 91 92 (2015) report that under mesophilic conditions, an average HRT in the range of 15-30 d is required to treat waste. 93

The experiment was started by filling R1 with 1.4 kg inoculum and 0.7 kg DCM, 94 R2 with 5.011 kg inoculum and 0.239 kg DCM, and R3 with 5.040 kg inoculum and 95 0.210 kg DCM. From the second day, all digesters were fed as follows: 0.7 kg, 0.239kg, 96 97 and 0.210 kg DCM for R1, R2, and R3, respectively (after the first removing of the same amount of digestate from a port at the base of the digesters) which continued for 98 the following 21 d adaptation period. The digesters were fed through a tube, the outlet 99 100 of which was submerged under the substrate level to avoid air ingress during the feeding process. Data were collected after this 21 d startup period. During the data 101 collection period, R1 was fed 0.7 kg DCM. Effluent from this digester (0.239 kg) was 102 103 used to feed R2, while R3 was fed 0.210 kg DCM. Digesters were kept at ambient temperature, and the experiment was run for a period of three HRT corresponding to 75 104 d in total. 105

107

Inoculum and Substrate

Inoculum in this study was obtained from the active biogas digester at the Faculty of Animal and Agricultural Sciences, Diponegoro University. The digester treats DCM and operates at ambient temperature. The digested slurry from the digester was transferred directly to the laboratory scale digesters.

The substrate was taken from dairy cows in the lactation period and was 112 collected from the farm in the Faculty of Animal and Agricultural Sciences, Diponegoro 113 University. Manure was diluted with tap water in the ratio of 1:1.5. Manure was 114 collected once per week and diluted with tap water directly and kept refrigerated. The 115 116 pH value, volatile solids (VS), and total ammonia nitrogen (TAN) concentration in the inoculum were 7.11, 7.33%, and 265.18 mg/L, respectively, while pH value, VS, TAN, 117 and volatile fatty acids (VFA) (C2-C5) concentrations of DCM were 6.77, 7.40%, 97.98 118 mg/L, and 142.93 mg/L respectively. 119

- 120
- 121

Analytical Methods

Biogas from the laboratory scale bio-digesters was passed up through 0.5 L 122 infusion bottles that contained 4% NaOH solution in order to absorb CO₂ using 5 mL 123 124 diameter Teflon tubing. Methane production was measured on a daily basis by collecting the gas using 5 L Tedlar gas bags using a water displacement method (Figure 125 1). The procedures to quantify gas production consisted of 6 steps. 1) The valve to 126 127 pump was in an open position. 2) The water pump was switched on, therefore, air in the measuring glass headspace was removed, and the headspace was filled up with tap 128 water. 3) The valve to pump was closed. 4) The water pump was switched off. 5) The 129

valve to Tedlar gas bag was opened therefore the methane in the Tedlar gas bag will move to the headspace of the measuring glass. 6) The gas volume was read in the measuring glass scale. When the gas volume in the Tedlar gas bag exceeded the measuring glass volume, then the steps 1-6 were repeated. The net gas production was corrected to STP conditions.

Daily maximum and minimum ambient temperatures were recorded using a 135 digital hygrometer thermometer HTC-2 (Taiwan). The sample pH value was measured 136 137 using a pH meter (Hanna® pH meter). Dry matter (DM) contents of samples were analyzed by drying at 105°C for 7 h. Ash was determined by combusting the dried 138 samples at 550°C for 6 h, and VS was calculated by subtracting the ash weight from the 139 140 DM (APHA,1995). TAN concentration was measured using photometric kits (HACH® USA: DOC316.53.01077) at 655 nm. VFA were determined using gas chromatography 141 (Shimadzu GC-8). The collected data were statistically analyzed manually using 142 ANOVA with 95% confidence level. Duncan's multiple range tests were used in post 143 ANOVA analysis when differences were found to be significant (Gomez & Gomez, 144 145 2007).

146

147

148

RESULTS

Ambient Temperature Variation

Average daily maximum-minimum ambient temperatures throughout the experiment were 36.55°C and 20.93°C, respectively (Figure 2). There was 15.63°C temperature difference between the maximum temperature in day time and minimum temperature in the night in this study.

153

| 154 | Methane Production |
|-----|--|
| 155 | The methane productions of the three bio-digesters throughout the experiment |
| 156 | are presented in Figure 3. The mean methane yields were 14.31 L/kg VS, 132.82 L/kg |
| 157 | VS, and 146 L/kg VS for R1, R2, and R3 respectively. The total methane yield of R1 |
| 158 | and R2 (R _{TS}) was 147.13 L/kg VS (Table 1). |
| 159 | |
| 160 | Variables in the Liquid Phase |
| 161 | Total VFA concentration and pH value of digested slurry are presented in Table |
| 162 | 1. The mean total VFA concentration was 160.74; 48.23; 39.19 mg/L for R1, R2, and |
| 163 | R3, respectively. Total VFA concentration of digested slurry in R1 was significantly |
| 164 | higher (p<0.05) than that in R2 and R3 (Table 1). TAN concentrations of digested slurry |
| 165 | in this study were 137.85; 178.96; and 185.86 mg/L for R1, R2, and R3, respectively |
| 166 | (Table 1). Volatile solid reductions in this study were 29.85 and 28.03% for R2 and R3, |
| 167 | respectively. |
| 168 | |
| 169 | DISCUSSION |
| 170 | Ambient Temperature Variation |
| 171 | This study was performed in July-September, and in Indonesia that period is |
| 172 | considered to be in the dry season. A large variation of temperatures in AD operation |
| 173 | were found during the course of this study that eventually had an adverse impact on the |
| 174 | microorganism activity. Mao et al. (2015) report that the AD process is carried out by a |
| 175 | prime balanced population of various microorganisms. These microorganisms are very |
| 176 | sensitive to environmental condition changes including temperature. Therefore, the |

ambient temperature in this study (Figure 2) falls into the mesophilic category (Burtonand Turner, 2003).

- 179
- 180

Methane Production

There was no significant effect of the application of a two-phase bio-digester on 181 specific methane yield in terms of kg VS of substrate added when compared to that 182 from the single digester configuration (Table 1). However, methane production of R_{TS} 183 was significantly higher (p<0.05) than that in R3 in terms of L/L digester volume 184 (methane production/volume active). The non-significant effect of the application of the 185 two-stage digester than single digester on specific methane yield in this study can be 186 187 due to the activities of anaerobic microorganisms in both reactor configurations operate efficiently. This study used digested slurry from an active digester that operated at a 188 tropical ambient temperature, the same condition used in this study. This fact, along 189 with the three weeks adaptation period, contributed to the efficient microorganism's 190 activity in both reactor configurations in this study even though there was a large 191 192 temperature difference between day and night time. A study by Chae et al. (2008) found that using batch digesters and treating swine manure, the methane production at 30 and 193 35°C were quite similar, but it was higher by more than 13%-17% than that at 25°C. 194 195 Temperature shocks caused a reduction in the methane production rate compared to that of the control, but it recovered rapidly. Once adapted, no significant effect on methane 196 production was observed between the control and the temperature shock bio-digester. 197 198 This fact therefore indicates that, even though methanogenic archaea are quite sensitive to temperature shock, they have considerable abilities to adapt to temperature changes 199 (Chae et al., 2008). 200

A study from Beneragama *et al.* (2013) using batch digesters with 16 d incubation period at 55°C showed that methane production of DCM was 145.03 L/kg VS while the study from Sutaryo *et al.* (2014) using continuous digesters with 20 d HRT at 35°C found that methane production of DCM was 177 L/kg VS. Both studies were performed at a constant mesophilic temperature while the study presented here was performed at ambient variable mesophilic temperatures. However, the result of this study is similar to those of previous results.

208 Methane production in terms of digester volume of R_{TS} was 29.98% higher than 209 that in R3. The positive effect (p < 0.05) of the application of two-phase digestion on the 210 methane production compared to that in the single-phase reactor can be attributed to a 211 shorter HRT period in R1 and R2 than that in R3, therefore the amounts of substrate added to R1 and R2 were higher than that in R3. Since the amount of substrate added to 212 R2 (0.239 kg) was higher than that in R3 (0.210 kg) and in the same time, the active 213 volumes in both digester configurations were equal (5.25 L) therefore methane 214 production in term of digester volume R2 was higher than that in R3. In fact, methane 215 216 production in R_{TS} was the summation of methane yields in R1 and in R2. In this present study, HRT in R1, R2, and R3 were 3 d, 22 d, and 25 d, respectively. Sinbuathong et al. 217 (2012) reported that one of the advantages of phase separation is the ability to handle a 218 219 higher organic loading rate than that in a single reactor. A similar study from Tsigkou et al. (2020) found the same phenomenon, in that the application of a two-stage digester 220 treating co-digestion of used disposable nappies and expired food product at 60:40 (v/v)221 222 ratio, working at mesophilic condition (37±0.5°C) and 15 d HRT, the energy production was 18.5% higher than that in the single reactor. 223

224

Variables in the Liquid Phase

225 During the bioconversion of organic matter in AD system, there are four steps, 226 namely hydrolysis, acidogenesis, acetogenesis, and methanogenesis. In a two-stage 227 digester configuration, the first digester serves as the acidogenic phase (Sinbuatong et al., 2012), therefore the VFA concentration will be higher than that in the second 228 digester. A higher total VFA concentration in R1 than that on the other reactor in this 229 study is in accordance with the report of Baldi et al. (2019), who found that the total 230 VFA concentration of digested slurry in a fermentative digester was significantly higher 231 232 than that of digested slurry from methanogenic digester.

The higher VFA concentration of R1-digested slurry gave consequences on the lower pH value (p<0.05) than those in R2 and R3-digested slurry. The mean pH values of digested slurry in this recent study were 6.46; 6.84, and 6.89 for R1, R2, and R3, respectively. The pH values of R2 and R3 in this recent study were in the range of a stable AD process. Mao *et al.* (2015) report that the ideal pH value for AD process is in the range of 6.8 to 7.4.

Ammonia is one of the essential nutrients for the growth of microorganisms, 239 240 however, it can inhibit the AD process if it is available at high concentrations (Yenigün and Demirel, 2013). Under mesophilic conditions (35°C), the TAN inhibitory threshold 241 242 was in the concentrations of around 1700-1800 mg/L for unacclimated inoculum 243 (Yenigün & Demirel, 2013). The TAN concentration of digested slurry in R1 was significantly lower (p<0.05) than those in R2 and R3. This fact can be attributed to a 244 shorter HRT in R1 than those in R2 and R3 therefore, microorganisms in R2 and R3 can 245 246 degrade more protein in the substrate, subsequently producing more ammonia. However, TAN concentrations of digested slurry from all digester in this study were 247 below the inhibitory level reported by Yenigün & Demirel (2013). 248

There was no significant effect of the application of two stages compared to 249 single stage digester on the VS reduction. No significant effect of phase separation on 250 volatile solid reduction in this study suggests that microorganisms in both reactor 251 configurations can work well. Brown and Li (2013) found VS reductions of 27% and 252 33% for the batch of AD, treating yard waste and combination of 90% yard waste and 253 10% food waste, respectively, and maintained at 36°C for 30 d. Meanwhile, a study 254 from Sutaryo et al. (2012) found a VS reduction in the range of 27-35% for a reactor 255 256 treating DCM with different TS concentrations. Therefore, the result of this study is in accordance with the result of the previous study. 257

- 258
- 259

CONCLUSION

It has been demonstrated that the application of a two-phase digester treating 260 DCM working at a tropical ambient temperature significantly increased methane 261 production by 29.98% compared to the single stage reactor in terms of digester volume. 262 However, there was no positive effect of this digester configuration on specific methane 263 264 yield in terms of VS. Both digester configurations can run properly with stable methane production, low VFA, and TAN concentrations. Therefore the two-phase digester 265 configuration in tropical ambient temperature can be applied to increase methane 266 267 production in terms of digester volume.

- 268
- 269

CONFLICT OF INTEREST

We certify that there is no conflict of interest with any financial, personal, or other relationships with other people or organizations related to the material discussed in the manuscript.

| 273 | |
|-----|---|
| 274 | ACKNOWLEDGEMENT |
| 275 | The authors would like to thank Diponegoro University (grant number: |
| 276 | 109/UN7.5.5/PP/2018) for financing this study. |
| 277 | |
| 278 | REFERENCES |
| 279 | Adekunle, K. F. & J. A. Okolie. 2015. A review of biochemical process of anaerobic |
| 280 | digestion. Adv. Biosci. Biotechnol. 6:205-212. https://doi.org/10.4236/abb.2015.63020 |
| 281 | APHA. 1995. Standard Methods for Examination of Water and Waste Water. 19th Ed. |
| 282 | American Public Health Association, Washington DC. |
| 283 | Bandara, W. M. K. R. T. W., T. Kindaichi, H. Satoh, M. Sasakawa, Y. Nakahara, |
| 284 | M. Takahashi, & S. Okabe. 2012. Anaerobic treatment of municipal wastewater at |
| 285 | ambient temperature: Analysis of archaeal community structure and recovery of |
| 286 | dissolved methane. Water Res. 46: 5756-5764. |
| 287 | https://doi.org/10.1016/j.watres.2012.07.061 |
| 288 | Baldi, F., L. Pecorini, & R. Iannelli. 2019. Comparison of single-stage and two-stage |
| 289 | anaerobic co-digestion of food waste and activated sludge for hydrogen and methane |
| 290 | production. Renew Energy. 43:1755-1765. https://doi.org/10.1016/j.renene.2019.05.122 |
| 291 | Beneragama, N., S. A. Lateef, M. Iwasaki, T. Yamashiro, & K. Umetsu. 2013. The |
| 292 | combined effect of cefazolin and oxytetracycline on biogas production from |
| 293 | thermophilic anaerobic digestion of dairy manure. Bioresour. Biotechnol. 133:23-30. |
| 294 | https://doi.org/10.1016/j.biortech.2013.01.032 |

Burton, C.H. & Turner, C. 2003. Anaerobic treatment options for animal manures. In:
Manure Management - Treatment Strategies for Sustainable Agriculture, 2nd Ed, chapter
7. Silsoe Research Institute, as part of the EU Accompanying Measure project,
MATRESA, Wrest Park, Silsoe, Bedford, UK.

- Brown, D. & Y. Li. 2013. Solid state anaerobic co-digestion of yard waste and food
 waste for biogas production. Bioresour. Technol. 127: 275-280.
 https://doi.org/10.1016/j.biortech.2012.09.081
- 303 Chae, K. J., S. K. Am Jang, L. Yim, & S. Kim. 2008. The effects of digestion
 304 temperature and temperature shock on the biogas yields from the mesophilic anaerobic
 305 digestion of swine manure. Bioresour. Technol. 99: 1-6.
 306 https://doi.org/10.1016/j.biortech.2006.11.063
- Ganesh, R., M. Torrijos, P. Sousbie, A. Lugardon, J. P. Steyer, & J. P. Delg. 2014.
 Single-phase and two-phase anaerobic digestion of fruit and vegetable waste:
 Comparison of start-up, reactor stability and process performance. Waste Manag. 34:
 875-885. https://doi.org/10.1016/j.wasman.2014.02.023
- Gomez, K. A., & A. A. Gomez. 2007. Prosedur Statistik untuk Penelitian Pertanian.
 Translated by Sjamsuddin, E., & J. S. Baharsjah. UI Press, Jakarta.
- Linke, B., A. Rodríguez-Abalde, C. Jost, & A. Krieg. 2015. Performance of a novel
 two-phase continuously fed leach bed reactor for demand-based biogas production from

- 315
 maize
 silage.
 Bioresour.
 Technol.
 177:
 34-40.

 316
 https://doi.org/10.1016/j.biortech.2014.11.070
- Mao, C., Y. Feng, X. Wang, & G. Ren. 2015. Review on research achievements of
 biogas from anaerobic digestion. Renew. Sust. Energ. Rev. 45: 540-555.
 https://doi.org/10.1016/j.rser.2015.02.032
- Minale, M. & T. Worku. 2014. Anaerobic co-digestion of sanitary wastewater and
 kitchen solid waste for biogas and fertilizer production under ambient temperature:
 waste generated from condominium house. Int. J. Environ. Sci. Technol. 11: 509-516.
 https://doi.org/10.1007/s13762-013-0255-7
- 324 Murugan, N. & P. Appavu. 2018. Investigation on low temperature biogas generation.
- 325 Int. J. ambient energy. 39:1-3. https://doi.org/10.1080/01430750.2018.1443283
- 326 Noorollahi, Y., M. Kheirrouz, H. F. Asl, H. Yousefi, & A. Hajinezhad. 2015. Biogas
- 327 production potential from livestock manure in Iran. Renew. Sust. Energ. Rev. 50: 748-
- 328 754. https://doi.org/10.1016/j.rser.2015.04.190
- Rao, P. V., S. S. Baral, R. Dey, & S. Mutnuri. 2010. Biogas generation potential by
 anaerobic digestion for sustainable energy development in India. Renew. Sust. Energ.
 Rev. 14: 2086-2094. https://doi.org/10.1016/j.rser.2010.03.031
- 332 Sinbuathong, N., P. Sirirote, B. Sillapacharoenkul, J. Munakata-Marr, & S. Chulalaksananukul. 2012. Biogas production from two-stage anaerobic digestion of 333 cake. Source 34: 2048-2056. 334 jatropa curcas seed Energ. Part A. 335 https://doi.org/10.1080/15567036.2012.664947

Sutaryo, S., A. J. Ward, & H. B. Møller. 2012. Thermophilic anaerobic co-digestion
of separated solids from acidified dairy cow manure. Bioresour. Technol. 114: 195-200.
https://doi.org/10.1016/j.biortech.2012.03.041

- 339 Sutaryo, S., A. J. Ward, & H. B. Møller. 2014. The effect of mixed-enzyme addition
- in anaerobic digestion on methane yield of dairy cattle manure. Environ. Technol. 35:
- 341 2476-2482. https://doi.org/10.1080/09593330.2014.911356
- 342 Tsigkou, K., P. Tsafrakidou, A. Kopsahelis, D. Zagklis, C. Zafiri, & M. Kornaros.
- 343 2020. Used disposable nappies and expired food products valorization through one- &

two-stage anaerobic co-digestion. Renew. Energy. 147: 610-619.
https://doi.org/10.1016/j.renene.2019.09.028

- Wei, S., H. Zhang, Z. Cai, J. Xu, J. Fang, & H. Liu. 2014. Psychrophilic anaerobic
 co-digestion of highland barley straw with two animal manures at high altitude for
 enhancing biogas production. Energy convers. manag. 88: 40-48.
 https://doi.org/10.1016/j.enconman.2014.08.018
- Yenigün, O. & B. Demirel. 2013. Ammonia inhibition in anaerobic digestion: A
 review. Process Biochem. 48: 901-911. https://doi.org/10.1016/j.procbio.2013.04.012



- 1. Tap water
- 2. Water container
- 3. Measuring glass
- 4. Measuring glass holder
- 5. Teflon tube Ø 5 mm
- Valve to pump and valve to tedlar gas bag
- 7. Water pump
- 8. Switch
- 9. Tedlar gas bag



365 Figure 2. Maximum-minimum ambient temperatures during experiment. ■: maximum,

▲ : minimum.


Time (d)



Figure 3. A. Methane yield per kg VS added. B. Methane yield per digester volume per

372 day.
$$\blacktriangle$$
: R1, \blacklozenge : R2, \times : R3, *:R_{TS}.

376

| Reacto | ors | Variables | | | | | | | | | |
|-----------------|--|---|---------------------|---------------------------|---------------------------|-------------------------|------------------------|--|--|--|--|
| | | Methane yield | | Total VFA | TAN | VS | pH | | | | |
| | | | | | | reduction | | | | | |
| | (L/kg | VS) | (L/L/d) | (mg/L) | (mg/L) | (%) | | | | | |
| R1 | 14.3 | 1±2.29 | 0.08±0.01 | 160.74±58.95 ^a | 137.84±45.32 ^a | | 6.46±0.17 ^a | | | | |
| R2 | 132.82 | ±33.92 | 0.32±0.07 | 48.23±23.73 ^b | 178.96±23.61 ^b | 29.85±6.76 ^a | 6.84±0.17 ^b | | | | |
| R3 | 146.65 | ±42.47 | $0.31{\pm}0.08^{a}$ | 39.19±23.23 ^b | 185.86±23.68 ^b | 28.03±3.19 ^a | 6.90±0.28 ^b | | | | |
| R _{TS} | 147.13 | ±34.29 | 0.41 ± 0.07^{b} | | | | | | | | |
| 378 | Note: VFA= | Volatile | fatty acid; TA | N= Total ammo | nia nitrogen; VS= | = Volatile solid | l; | | | | |
| 379 | R1= | R1= First reactor of the two-phase digester; R2= Second reactor of the two- | | | | | | | | | |
| 380 | phase | phase bio-digester; R3= Single-phase reactor, R _{TS:} Total sum methane yield of | | | | | | | | | |
| 381 | R1 and R2. Means in the same column with different superscripts differ | | | | | | | | | | |
| 382 | signi | significantly (p<0.05). | | | | | | | | | |
| 383 | | | | | | | | | | | |
| 384 | | | | | | | | | | | |
| 385 | | | | | | | | | | | |
| 386 | | | | | | | | | | | |

377Table 1. Methane yield, Total VFA, TAN, VS reduction, and pH of some reactorsReactorsVariables

10. Permintaan proofreading draft sebelum naskah terbit





Dear S. Sutaryo, A. N. Sempana, C. M. S. Lestari, A. J. Ward:

I am pleased to inform you that your article submitted to Tropical Animal Science Journal, entitled: "Performance Comparison of Single and Two-Phase Biogas Digesters Treating Dairy Cattle Manure at Tropical Ambient Temperature" has been approved to be published in Tropical Animal Science Journal in the upcoming edition. Please find the PROOF of your manuscript in the attached file. If there are still any corrections in the manuscript, please respond and return the document within 5 days.

Thank you for your article submission, and we are looking forward to receiving your incoming articles.

Prof. Dr. Komang G Wiryawan Chief Editor Tropical Animal Science Journal kgwiryawan@yahoo.com

...

.....

11. Penulis menyetujui versi proofreading

Sutaryo To: Tropical Animal Science Journal «mediapeternakan@apps.ipb.ac.id»
Dear Prof. Dr. Komang G. Wiryawan Chief Editor Tropical Animal Science Journal
Thank you for the proof read off my accepted article. I have read through the article and I found no error on it. Therefore I do agree to the

proof read article version.

Thank you and best regards,

On behalf of all the authors,

Sutaryo Sutaryo Dept. of Animal Science Faculty Animal and Agricultural Sciences Diponegoro University Kampus Tembalang 50275 Email: <u>sceta@lecturer.undip.ac.id</u>

.....

12. Draft memasuki proses produksi untuk penerbitan



Faculty of Animal Science Building. Bogor Agricultural University Jin. Agatis, Kampus IPB Darmaga, Bogor 16680, Indonesia Phone/Fax: +62-251-8421692 e-mail: <u>mediapeternakan@apos.iob.ac.id; mediapeternakan@yahoo.co.id</u> Website: <u>http://mediapeternakan@yahoo.co.id</u> Website: <u>http://mediapeternakan@index.ohp/tasj</u> Old website: <u>http://mediapeternakan.id/index.ohp/tasj</u>

13. Naskah publikasi terbit

Performance Comparison of Single and Two-Phase Biogas Digesters Treating Dairy Cattle Manure at Tropical Ambient Temperature

S. Sutaryo^{a,*}, A. N. Sempana^a, C. M. S. Lestari^a, & A. J. Ward^b

 ^aDepartment of Animal Science, Faculty of Animal and Agricultural Sciences, Diponegoro University, Jalan Prof. Soedarto, SH Tembalang Semarang, Kotak Pos 1269, Indonesia
 ^bDepartment of Engineering, Faculty of Science and Technology, Aarhus University, Aarhus, Denmark *Corresponding author: soeta@lecturer.undip.ac.id; sutaryoundip@yahoo.com (Received 14-04-2020; Revised 03-07-2020; Accepted 15-07-2020)

ABSTRACT

The biodegradation process of organic waste in anaerobic digestion can be in a single or two-phase bio-reactor. This study examined the effect of different biogas digester configurations (single and two-phase) on methane production of dairy cattle manure (DCM) at tropical ambient temperature. Three identical reactors were used in this study (R1, R2, and R3). The two-phase digesters consisted of reactors R1 and R2. R1 had a 2.1 L working volume and 3 d hydraulic retention time (HRT), while R2 had 5.25 L working volume and 22 d HRT (R1 and R2 had a 25 d HRT). The digested slurry of R1 was used to feed R2. R3 served as the single-phase digester and had 5.25 L working volume and 25 d HRT. Methane production were 14.31, 132.82, and 146 L/kg VS for R1, R2, and R3, respectively. The results showed that there was no positive effect of the application of a two-phase digester configuration on the specific methane yield of DCM per kg volatile solids added than that in the single-reactor. Methane production was detected in the first reactor of the two-phase digester configuration and the total methane production of the two-phase digester was found to be 29.98% higher (p<0.05) than that of the single reactor in terms of digester volume (0.41 VS 0.31 L/L/d). Both digester configurations performed well, indicated by a stable methane production and low volatile fatty acids and total ammonia concentrations. The two-phase bio-digester configuration can significantly increase methane production in terms of digester volume.

Keywords: biogas; manure; tropical ambient temperature; two-phase digester biogas

INTRODUCTION

The dairy cattle industry produces large amounts of waste in the form of manure that can cause environmental pollution if it is not managed properly. Daily dairy cattle manure (DCM) (wet feces plus urine) excretion is 2226.5 kg/year per 610 kg of body weight (Noorollahi *et al.*, 2015). Generally, animal waste management can take place in aerobic conditions through a composting process or by anaerobic digestion (AD) to produce biogas.

Manure management through the AD process results in numerous advantages, including the generation of renewable energy in the form of biogas. Biogas is the most efficient and effective among the various alternative sources of energy currently available, it needs less capital investment per unit production cost compared to the other renewable energy sources, and it is available as a domestic resource in the rural areas. Therefore, it is not subject to world price fluctuations (Rao *et al.*, 2010). In addition, biogas production from animal manure can create new enterprises and increases the income in a rural area since it requires labor for production, collection and transport of AD substrates, manufacture of technical equipment and the construction, operation, and maintenance of biogas plants (Adekunle & Okolie, 2015).

Technically, the AD process can take place in three different temperature ranges: (1) psychrophilic (cryophilic) temperature from 10°C to 20°C; (2) mesophilic temperature from 20°C to 40°C; and (3) thermophilic temperature from 40°C to 60°C (Burton & Turner, 2003). Based on those temperature-range criteria, the AD process can be implemented at tropical ambient temperatures. Moreover, the operation of AD at tropical ambient temperatures offers advantages compared to the operation of AD under mesophilic or thermophilic temperatures since AD operation at higher temperatures requires a significant amount of energy to maintain bioreactor temperature (Bandara *et al.*, 2012).

Among the other biogas-digester designs, the continuously stirred-tank reactor (CSTR) design is the most commonly applied bioreactor for treating agricultural waste (Linke *et al.*, 2015). While in operation, the process of biodegradation of organic waste can be in single or two-phases. The two-phase AD process has several advantages compared to a single phase. These include the selection and enrichment of different bacteria in each digester, increasing the stability of the process by controlling the acidification stage, therefore reducing the risk of overloading and the build up of toxic material. The first stage in the two-phase configuration can act as a metabolic buffer preventing pH shock to the methanogenic microorganisms and low pH in the first stage since a high organic loading rate favors the establishment of the acidogenic phase (Sinbuathong et al., 2012). On the other hand, single-phase biodigester has also advantageous as it is a simple and straightforward operation and for an easier degradable substrate such as fruit and vegetable waste, single-phase process could be the preferred choice rather than two-phase reactor (Ganesh et al., 2014). Although previous studies have evaluated the AD process at ambient temperature (Minale & Worku, 2014; Wei et al., 2014; Murrugan & Appavu, 2018) and two-phase AD (Baldi et al., 2019; Tsigkou et al., 2020), to the best of our knowledge there has been a lack of information regarding to a direct comparison of single and two-phase AD of DCM in tropical ambient temperature. Therefore, the aim of this current study was to evaluate the process performance of single and two-phase biodigesters treating DCM and working in this specific area.

MATERIALS AND METHODS

Experimental Set-Up

Evaluation of single and two-phase processes was conducted using three identical digesters, namely R1, R2, and R3. The reactors were made from stainless steel, and in order to minimize temperature fluctuations between day and night times, all digesters were made with double layers. The two-phase digesters consisted of reactors R1 and R2. Reactor 1 had a 2.1 L working volume (the minimum volume that can be applied in the reactor) and 3 d hydraulic retention (HRT), while R2 had 5.25 L working volume and 22 d HRT. Therefore in total, R1 and R2 had a 25 d HRT. R3 served as the single-phase bioreactor and had 5.25 L working volume and 25 d HRT. Mao *et al.* (2015) report that under mesophilic conditions, an average HRT in the range of 15-30 d is required to treat waste.

The experiment was started by filling R1 with 1.4 kg inoculum and 0.7 kg DCM, R2 with 5.011 kg inoculum and 0.239 kg DCM, and R3 with 5.040 kg inoculum and 0.210 kg DCM. From the second day, all digesters were fed as follows: 0.7 kg, 0.239kg, and 0.210 kg DCM

for R1, R2, and R3, respectively (after the first removing of the same amount of digestate from a port at the base of the digesters) which continued for the following 21 d adaptation period. The digesters were fed through a tube, the outlet of which was submerged under the substrate level to avoid air ingress during the feeding process. Data were collected after this 21 d startup period. During the data collection period, R1 was fed 0.7 kg DCM. Effluent from this digester (0.239 kg) was used to feed R2, while R3 was fed 0.210 kg DCM. Digesters were kept at ambient temperature, and the experiment was run for a period of three HRT corresponding to 75 d in total.

Inoculum and Substrate

Inoculum in this study was obtained from the active biogas digester at the Faculty of Animal and Agricultural Sciences, Diponegoro University. The digester treats DCM and operates at ambient temperature. The digested slurry from the digester was transferred directly to the laboratory scale digesters.

The substrate was taken from dairy cows in the lactation period and was collected from the farm in the Faculty of Animal and Agricultural Sciences, Diponegoro University. Manure was diluted with tap water in the ratio of 1:1.5. Manure was collected once per week and diluted with tap water directly and kept refrigerated. The pH value, volatile solids (VS), and total ammonia nitrogen (TAN) concentration in the inoculum were 7.11, 7.33%, and 265.18 mg/L, respectively, while pH value, VS, TAN, and volatile fatty acids (VFA) (C2-C5) concentrations of DCM were 6.77, 7.40%, 97.98 mg/L, and 142.93 mg/L respectively.

Analytical Methods

Biogas from the laboratory scale bio-digesters was passed up through 0.5 L infusion bottles that contained 4% NaOH solution in order to absorb CO_2 using 5 mL diameter Teflon tubing. Methane production was measured on a daily basis by collecting the gas using 5 L Tedlar gas bags using a water displacement method (Figure 1). The procedures to quantify gas production consisted of 6 steps. 1) The valve to pump was in an open position. 2) The water pump was switched on, therefore, air in the measuring glass headspace was re-



Figure 1. Apparatus for measuring gas production

moved, and the headspace was filled up with tap water. 3) The valve to pump was closed. 4) The water pump was switched off. 5) The valve to Tedlar gas bag was opened therefore the methane in the Tedlar gas bag will move to the headspace of the measuring glass. 6) The gas volume was read in the measuring glass scale. When the gas volume in the Tedlar gas bag exceeded the measuring glass volume, then the steps 1-6 were repeated. The net gas production was corrected to STP conditions.

Daily maximum and minimum ambient temperatures were recorded using a digital hygrometer thermometer HTC-2 (Taiwan). The sample pH value was measured using a pH meter (Hanna® pH meter). Dry matter (DM) contents of samples were analyzed by drying at 105°C for 7 h. Ash was determined by combusting the dried samples at 550°C for 6 h, and VS was calculated by subtracting the ash weight from the DM (APHA,1995). TAN concentration was measured using photometric kits (HACH® USA: DOC316.53.01077) at 655 nm. VFA were determined using gas chromatography (Shimadzu GC-8). The collected data were statistically analyzed manually using ANOVA with 95% confidence level. Duncan's multiple range tests were used in post ANOVA analysis when differences were found to be significant (Gomez & Gomez, 2007).

RESULTS

Ambient Temperature Variation

Average daily maximum-minimum ambient temperatures throughout the experiment were 36.55°C and 20.93°C, respectively (Figure 2). There was 15.63°C temperature difference between the maximum temperature in day time and minimum temperature in the night in this study.

Methane Production

The methane productions of the three bio-digesters throughout the experiment are presented in Figure 3. The mean methane yields were 14.31 L/kg VS, 132.82 L/kg VS, and 146 L/kg VS for R1, R2, and R3 respectively. The total methane yield of R1 and R2 ($R_{\rm TS}$) was 147.13 L/kg VS (Table 1).



Figure 2. Maximum-minimum ambient temperatures during experiment. ■: maximum, ▲: minimum.

Variables in the Liquid Phase

Total VFA concentration and pH value of digested slurry are presented in Table 1. The mean total VFA concentration was 160.74; 48.23; 39.19 mg/L for R1, R2, and R3, respectively. Total VFA concentration of digested slurry in R1 was significantly higher (p<0.05) than that in R2 and R3 (Table 1). TAN concentrations of digested slurry in this study were 137.85; 178.96; and 185.86 mg/L for R1, R2, and R3, respectively (Table 1). Volatile solid reductions in this study were 29.85 and 28.03% for R2 and R3, respectively.

DISCUSSION

Ambient Temperature Variation

This study was performed in July-September, and in Indonesia that period is considered to be in the dry season. A large variation of temperatures in AD operation were found during the course of this study that eventually had an adverse impact on the microorganism activity. Mao *et al.* (2015) report that the AD process is carried out by a prime balanced population of various microorganisms. These microorganisms are very sensitive to environmental condition changes including temperature. Therefore, the ambient temperature in this study (Figure 2) falls into the mesophilic category (Burton & Turner, 2003).



Figure 3. A. Methane yield per kg VS added. B. Methane yield per digester volume per day. ▲: R1, ◆: R2, ×: R3, *: RTS.

| | Variables | | | | | | | | |
|----------|---------------|---------------------|--------------------------|---------------------------|--------------|------------------------|--|--|--|
| Reactors | Methane yield | | Total VFA | TAN | VS reduction | | | | |
| | (L/kg VS) | (L/L/d) | (mg/L) | (mg/L) | (%) | рп | | | |
| R1 | 14.31±2.29 | 0.08 ± 0.01 | 160.74±58.95ª | 137.84±45.32ª | | 6.46±0.17 ^a | | | |
| R2 | 132.82±33.92 | 0.32±0.07 | 48.23±23.73 ^b | 178.96±23.61 ^b | 29.85±6.76 | 6.84±0.17 ^b | | | |
| R3 | 146.65±42.47 | 0.31 ± 0.08^{a} | 39.19±23.23 ^b | 185.86±23.68 ^b | 28.03±3.19 | 6.90±0.28 ^b | | | |
| RTS | 147.13±34.29 | 0.41 ± 0.07^{b} | | | | | | | |

Table 1. Methane yield, total VFA, TAN, VS reduction, and pH of some reactors

Note: VFA= Volatile fatty acid; TAN= Total ammonia nitrogen; VS= Volatile solid; R1= First reactor of the two-phase digester; R2= Second reactor of the two-phase bio-degester; R3= Single-phase reactor, RTS: Total sum methane yield of R1 and R2. Means in the same column with different superscripts differ significantly (p<0.05).

Methane Production

There was no significant effect of the application of a two-phase bio-digester on specific methane yield in terms of kg VS of substrate added when compared to that from the single digester configuration (Table 1). However, methane production of R_{TS} was significantly higher (p<0.05) than that in R3 in terms of L/L digester volume (methane production/volume active). The non significant effect of the application of the two-stage digester than single digester on specific methane yield in this study can be due to the activities of anaerobic microorganisms in both reactor configurations operate efficiently. This study used digested slurry from an active digester that operated at a tropical ambient temperature, the same condition used in this study. This fact, along with the three weeks adaptation period, contributed to the efficient microorganism's activity in both reactor configurations in this study even though there was a large temperature difference between day and night time. A study by Chae et al. (2008) found that using batch digesters and treating swine manure, the methane production at 30 and 35°C were quite similar, but it was higher by more than 13%-17% than that at 25°C. Temperature shocks caused a reduction in the methane production rate compared to that of the control, but it recovered rapidly. Once adapted, no significant effect on methane production was observed between the control and the temperature shock bio-digester. This fact therefore indicates that, even though methanogenic archaea are quite sensitive to temperature shock, they have considerable abilities to adapt to temperature changes (Chae et al., 2008).

A study from Beneragama *et al.* (2013) using batch digesters with 16 d incubation period at 55°C showed that methane production of DCM was 145.03 L/kg VS while the study from Sutaryo *et al.* (2014) using continuous digesters with 20 d HRT at 35°C found that methane production of DCM was 177 L/kg VS. Both studies were performed at a constant mesophilic temperature while the study presented here was performed at ambient variable mesophilic temperatures. However, the result of this study is similar to those of previous results.

Methane production in terms of digester volume of R_{TS} was 29.98% higher than that in R3. The positive effect (p<0.05) of the application of two-phase digestion on the methane production compared to that in the single-

phase reactor can be attributed to a shorter HRT period in R1 and R2 than that in R3, therefore the amounts of substrate added to R1 and R2 were higher than that in R3. Since the amount of substrate added to R2 (0.239 kg) was higher than that in R3 (0.210 kg) and in the same time, the active volumes in both digester configurations were equal (5.25 L) therefore methane production in term of digester volume R2 was higher than that in R3. In fact, methane production in R_{TS} was the summation of methane yields in R1 and in R2. In this present study, HRT in R1, R2, and R3 were 3 d, 22 d, and 25 d, respectively. Sinbuathong et al. (2012) reported that one of the advantages of phase separation is the ability to handle a higher organic loading rate than that in a single reactor. A similar study from Tsigkou et al. (2020) found the same phenomenon, in that the application of a twostage digester treating co-digestion of used disposable nappies and expired food product at 60:40 (v/v) ratio, working at mesophilic condition (37±0.5°C) and 15 d HRT, the energy production was 18.5% higher than that in the single reactor.

Variables in the Liquid Phase

During the bioconversion of organic matter in AD system, there are four steps, namely hydrolysis, acidogenesis, acetogenesis, and methanogenesis. In a twostage digester configuration, the first digester serves as the acidogenic phase (Sinbuatong *et al.*, 2012), therefore the VFA concentration will be higher than that in the second digester. A higher total VFA concentration in R1 than that on the other reactor in this study is in accordance with the report of Baldi *et al.* (2019), who found that the total VFA concentration of digested slurry in a fermentative digester was significantly higher than that of digested slurry from methanogenic digester.

The higher VFA concentration of R1-digested slurry gave consequences on the lower pH value (p<0.05) than those in R2 and R3-digested slurry. The mean pH values of digested slurry in this recent study were 6.46; 6.84, and 6.89 for R1, R2, and R3, respectively. The pH values of R2 and R3 in this recent study were in the range of a stable AD process. Mao *et al.* (2015) report that the ideal pH value for AD process is in the range of 6.8 to 7.4.

Ammonia is one of the essential nutrients for the growth of microorganisms, however, it can inhibit the AD process if it is available at high concentrations (Yenigün & Demirel, 2013). Under mesophilic conditions (35°C), the TAN inhibitory threshold was in the concentrations of around 1700–1800 mg/L for unacclimated inoculum (Yenigün & Demirel, 2013). The TAN concentration of digested slurry in R1 was significantly lower (p<0.05) than those in R2 and R3. This fact can be attributed to a shorter HRT in R1 than those in R2 and R3 therefore, microorganisms in R2 and R3 can degrade more protein in the substrate, subsequently producing more ammonia. However, TAN concentrations of digested slurry from all digester in this study were below the inhibitory level reported by Yenigün & Demirel (2013).

There was no significant effect of the application of two stages compared to single stage digester on the VS reduction. No significant effect of phase separation on volatile solid reduction in this study suggests that microorganisms in both reactor configurations can work well. Brown and Li (2013) found VS reductions of 27% and 33% for the batch of AD, treating yard waste and combination of 90% yard waste and 10% food waste, respectively, and maintained at 36°C for 30 d. Meanwhile, a study from Sutaryo *et al.* (2012) found a VS reduction in the range of 27-35% for a reactor treating DCM with different TS concentrations. Therefore, the result of this study is in accordance with the result of the previous study.

CONCLUSION

It has been demonstrated that the application of a two-phase digester treating DCM working at a tropical ambient temperature significantly increased methane production by 29.98% compared to the single stage reactor in terms of digester volume. However, there was no positive effect of this digester configuration on specific methane yield in terms of VS. Both digester configurations can run properly with stable methane production, low VFA, and TAN concentrations. Therefore the two-phase digester configuration in tropical ambient temperature can be applied to increase methane production in terms of digester volume.

CONFLICT OF INTEREST

We certify that there is no conflict of interest with any financial, personal, or other relationships with other people or organizations related to the material discussed in the manuscript.

ACKNOWLEDGEMENT

The authors would like to thank Diponegoro University (grant number: 109/UN7.5.5/PP/2018) for financing this study.

REFERENCES

- Adekunle, K. F. & J. A. Okolie. 2015. A review of biochemical process of anaerobic digestion. Adv. Biosci. Biotechnol. 6:205-212. https://doi.org/10.4236/abb.2015.63020
- APHA. 1995. Standard Methods for Examination of Water and

Waste Water. 19th Ed. American Public Health Association, Washington DC.

- Bandara, W. M. K. R. T. W., T. Kindaichi, H. Satoh, M. Sasakawa, Y. Nakahara, M. Takahashi, & S. Okabe. 2012. Anaerobic treatment of municipal wastewater at ambient temperature: Analysis of archaeal community structure and recovery of dissolved methane. Water Res. 46: 5756-5764. https://doi.org/10.1016/j.watres.2012.07.061
- Baldi, F., L. Pecorini, & R. Iannelli. 2019. Comparison of singlestage and two-stage anaerobic co-digestion of food waste and activated sludge for hydrogen and methane production. Renew Energy. 43:1755-1765. https://doi.org/10.1016/j. renene.2019.05.122
- Beneragama, N., S. A. Lateef, M. Iwasaki, T. Yamashiro, & K. Umetsu. 2013. The combined effect of cefazolin and oxytetracycline on biogas production from thermophilic anaerobic digestion of dairy manure. Bioresour. Biotechnol. 133:23-30. https://doi.org/10.1016/j.biortech.2013.01.032
- Burton, C.H. & C. Turner. 2003. Anaerobic treatment options for animal manures. In: Manure Management - Treatment Strategies for Sustainable Agriculture, 2nd Ed, chapter 7. Silsoe Research Institute, as part of the EU Accompanying Measure project, MATRESA, Wrest Park, Silsoe, Bedford, UK.
- Brown, D. & Y. Li. 2013. Solid state anaerobic co-digestion of yard waste and food waste for biogas production. Bioresour. Technol. 127: 275-280. https://doi.org/10.1016/j. biortech.2012.09.081
- Chae, K. J., S. K. Am Jang, L. Yim, & S. Kim. 2008. The effects of digestion temperature and temperature shock on the biogas yields from the mesophilic anaerobic digestion of swine manure. Bioresour. Technol. 99: 1-6. https://doi. org/10.1016/j.biortech.2006.11.063
- Ganesh, R., M. Torrijos, P. Sousbie, A. Lugardon, J. P. Steyer,
 & J. P. Delg. 2014. Single-phase and two-phase anaerobic digestion of fruit and vegetable waste: Comparison of start-up, reactor stability and process performance. Waste Manag. 34: 875-885. https://doi.org/10.1016/j. wasman.2014.02.023
- Gomez, K. A. & A. A. Gomez. 2007. Prosedur Statistik untuk Penelitian Pertanian. Translated by Sjamsuddin, E., & J. S. Baharsjah. UI Press, Jakarta.
- Linke, B., A. Rodríguez-Abalde, C. Jost, & A. Krieg. 2015. Performance of a novel two-phase continuously fed leach bed reactor for demand-based biogas production from maize silage. Bioresour. Technol. 177: 34-40. https://doi. org/10.1016/j.biortech.2014.11.070
- Mao, C., Y. Feng, X. Wang, & G. Ren. 2015. Review on research achievements of biogas from anaerobic digestion. Renew. Sust. Energ. Rev. 45: 540-555. https://doi.org/10.1016/j. rser.2015.02.032
- Minale, M. & T. Worku. 2014. Anaerobic co-digestion of sanitary wastewater and kitchen solid waste for biogas and fertilizer production under ambient temperature: waste generated from condominium house. Int. J. Environ. Sci. Technol. 11: 509-516. https://doi.org/10.1007/s13762-013-0255-7
- Murugan, N. & P. Appavu. 2018. Investigation on low temperature biogas generation. Int. J. ambient energy. 39:1-3. https://doi.org/10.1080/01430750.2018.1443283
- Noorollahi, Y., M. Kheirrouz, H. F. Asl, H. Yousefi, & A. Hajinezhad. 2015. Biogas production potential from livestock manure in Iran. Renew. Sust. Energ. Rev. 50: 748-754. https://doi.org/10.1016/j.rser.2015.04.190
- Rao, P. V., S. S. Baral, R. Dey, & S. Mutnuri. 2010. Biogas generation potential by anaerobic digestion for sustainable energy development in India. Renew. Sust. Energ. Rev. 14: 2086-2094. https://doi.org/10.1016/j.rser.2010.03.031
- Sinbuathong, N., P. Sirirote, B. Sillapacharoenkul, J. Munakata-Marr, & S. Chulalaksananukul. 2012. Biogas

production from two-stage anaerobic digestion of jatropa curcas seed cake. Energ. Source Part A. 34: 2048-2056. https://doi.org/10.1080/15567036.2012.664947

- Sutaryo, S., A. J. Ward, & H. B. Møller. 2012. Thermophilic anaerobic co-digestion of separated solids from acidified dairy cow manure. Bioresour. Technol. 114: 195-200. https://doi.org/10.1016/j.biortech.2012.03.041
- Sutaryo, S., A. J. Ward, & H. B. Møller. 2014. The effect of mixed-enzyme addition in anaerobic digestion on methane yield of dairy cattle manure. Environ. Technol. 35: 2476-2482. https://doi.org/10.1080/09593330.2014.911356

Tsigkou, K., P. Tsafrakidou, A. Kopsahelis, D. Zagklis, C.

Zafiri, & M. Kornaros. 2020. Used disposable nappies and expired food products valorization through one- & two-stage anaerobic co-digestion. Renew. Energy. 147: 610-619. https://doi.org/10.1016/j.renene.2019.09.028

- Wei, S., H. Zhang, Z. Cai, J. Xu, J. Fang, & H. Liu. 2014. Psychrophilic anaerobic co-digestion of highland barley straw with two animal manures at high altitude for enhancing biogas production. Energy convers. manag. 88: 40-48. https://doi.org/10.1016/j.enconman.2014.08.018
- Yenigün, O. & B. Demirel. 2013. Ammonia inhibition in anaerobic digestion: A review. Process Biochem. 48: 901-911. https://doi.org/10.1016/j.procbio.2013.04.012